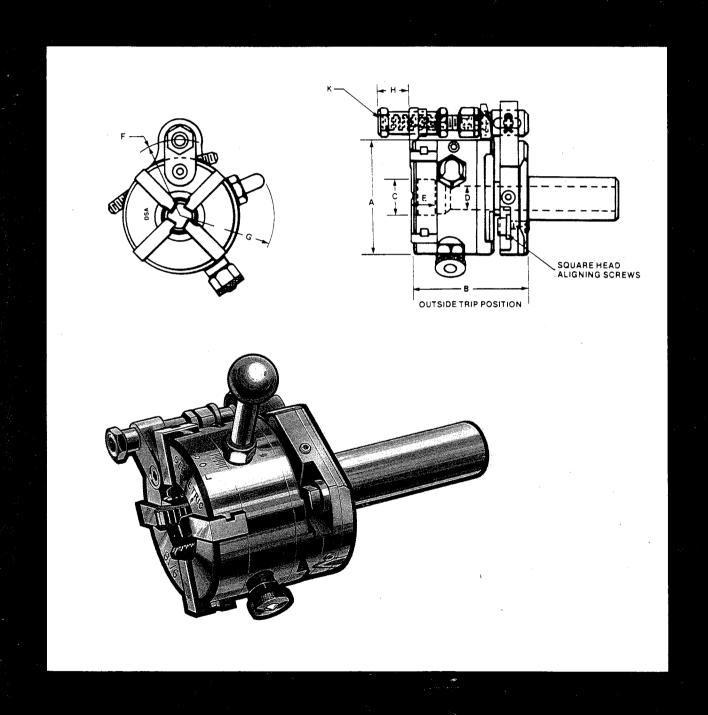
Geometric Standard Screw Threading Manual







The Distributor's Role... An Essential One.

No one works harder for you and for us than our local industrial tool distributor. First of all, we can say with pride that your Geometric distributor has taken care to provide you with the highest quality tools by selecting the Geometric line.

Without the many services the industrial distributor provides, industry would be in chaos. He has an intimate understanding of his customers' problems and his suppliers' capabilities and with that knowledge he can accurately bridge the gap between the tool user and the tool manufacturer. He provides prompt service and fast delivery. He functions as a warehouse, bookkeeper, banker and trucker to both the tool manufacturer and the end user. His knowledge of his customers' problems and methods makes it possible for him to provide the tool manufacturer with a clear picture of these problems and thus effect a quick remedy.

To the purchasing agent, whose job it is to exercise judgment as to quality and price of a vast range of industrial requirements, the distributor salesman can be of enormous value. He can provide the purchasing agent with detailed and reliable information on the products he sells.

It is with admiration and gratitude we say to our distributors, "Thank you and a hearty well done."

The
purpose of
this Handbook
is to help you to get
the type of production
from your GEOMETRIC
TOOLS that they are capable of
giving under proper operating
conditions.

From experience we have found that a sound fundamental knowledge of the tools and of their proper installation, operation, and care not only will avoid trouble but will pay in increased efficiency.

We hope you will read this book in its entirety so that, when occasion demands, you will know where to turn in it for help in instructing new operators, correcting threading errors or saving yourself the trouble of calling in a service engineer. And, last but not least, to so familiarize yourself with these versatile tools that you may quickly adapt them to new jobs or new requirements as they develop.

Geometric®Greenfield Industries, Inc.
470 Old Evans Road
Augusta, GA 30809

GEOMETRIC SCREW thread cutting manual

THE GEOMETRIC LINE OF TOOLS

On these two pages are shown the various types of threading tools in the GEOMETRIC line.

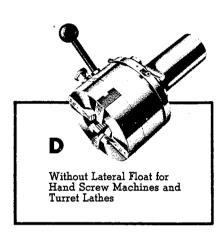
Each style of Die Head or Tap is made in a variety of sizes to accommodate different threading requirements, so no matter what type of machine you have available or what your threading problem, there is a GEOMETRIC tool to fit most any condition.

For complete specifications and price information regarding any tool illustrated, send for detailed Bulletin.



SELF OPENING

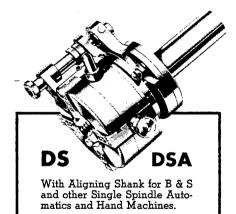
STATIONARY



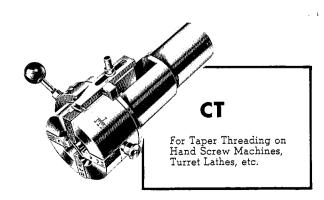


Acme, B & O, Foster, Gisholt, Libby, J & L and Warner & Swasey Turret Lathes etc.





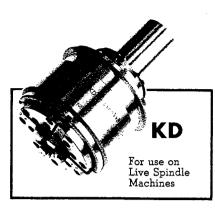






SELF OPENING

ROTARY





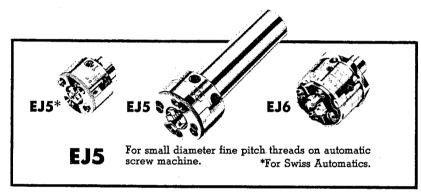
Similar in design to style KD — but employing five chasers.

CK

Similar in design to the Style KD — but employing smaller, lighter chasers. Designed for cutting finer pitch threads.

DIE HEADS - SOLID ADJUSTABLE

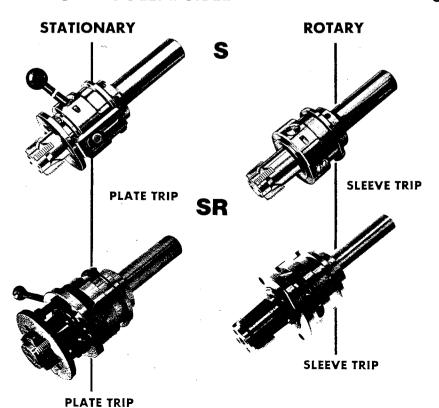
FOR ROTARY OR STATIONARY APPLICATIONS

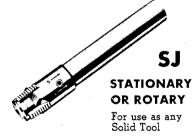




TAPS COLLAPSIBLE

SOLID ADJUSTABLE





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die heads



GENERAL INSTRUCTIONS

INSTALLING IN TURRET

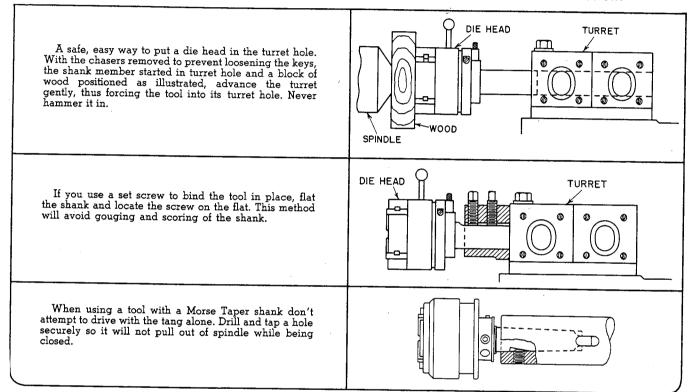
A self-opening die head is a precision tool. In order to produce accurate threads it must be kept in good condition and handled with care at all times. Proper installation of the head in the machine is of utmost importance as many threading faults may be traced to improper installation.

When putting the tool into the turret wipe out the hole to be sure there are no chips or dust.

Keep the shank clean and free from set screw

marks. Bind the shank in the turret securely but do not bear down so as to mar or gouge the shank. The shank of the tool, remember, locates the tool in relation to the work. A badly worn or bent shank means misalignment. Don't gouge into the shank if you value accurate threads or long tool life.

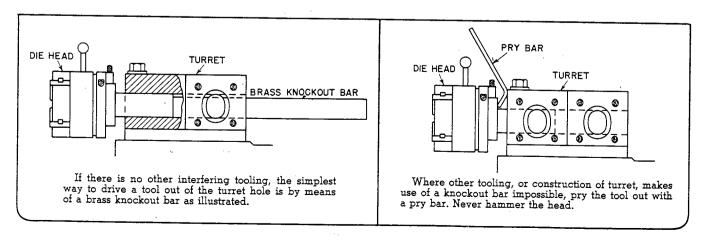
A few simple methods of putting a tool into the turret — without danger of damaging the tool or scoring the shank — are illustrated below.



REMOVING FROM TURRET

The reasons for care when installing a tool are equally applicable when removing it from the machine. Use special care that the tool does not drop

into the bed of the machine or on the floor as "internal injuries" not easily detected may result.



SETTING STOP ON MACHINE FOR THREAD LENGTH

The principle of a self-opening die head is to open at the end of the cut releasing the chasers from the work, thus permitting return of the die head without reversing the spindle.

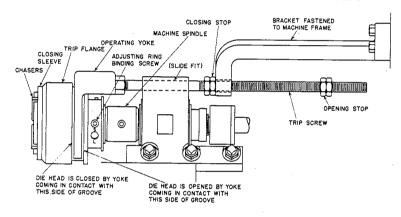
With a turret lathe, a stop is usually employed to stop the advance of the turret and allow the tool to be tripped at the predetermined length of thread. With automatic screw machines using rotary die heads, a yoke or fork is usually employed. In any case be sure the necessary adjustment is made prior to cutting a thread or you are apt to break chasers and even wreck the die head by running it into a shoulder or into the collet or chuck.

When setting a stop, keep in mind (1) the length of thread to be cut, (2) safety of the Die Head and Chasers.

Types of Stops and Closers

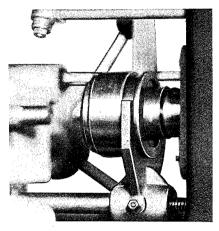
Most Geometric Heads have integral stop mechanisms or are hand operated. In some cases it will be necessary to provide stopping or closing mechanisms related to the machine set up. Below are a couple of typical arrangements.

ROTARY TYPE



SETTING OPERATING YOKE ON AUTOMATICS

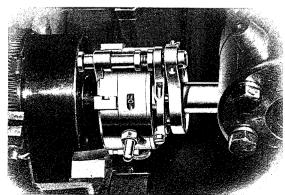
The drawing shows a typical example of how a Rotary Die head is operated on a multiple spindle automatic screw machine. The opening and closing of the head are controlled by adjusting the location of the nuts on the trip rod as shown. To prevent sluggish opening action the yoke should be narrow enough so that forward side of groove will not contact yoke when head trips.



FLANGE TRIP

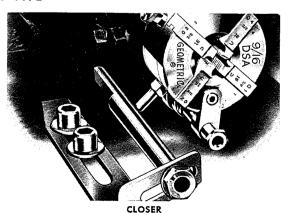
A single yoke operating in the groove of the trip flange opens and closes the die head.

STATIONARY TYPE



OUTSIDE TRIP ENGAGED

Note that outside trip gage contacts the spindle guard on machine when tripping.



This closer may be purchased from Brown & Sharpe Manufacturing Company, Providence, R.I.



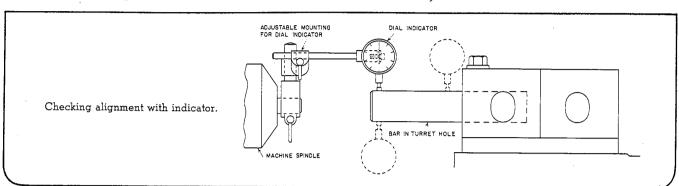
GENERAL INSTRUCTIONS

ALIGNMENT

Alignment of machine is one of the most important requirements of accurate screw thread cutting. When a die head is in true alignment with the work, all chasers of a set contact the work at the same time and the cutting of the thread is equally distributed among all the chasers of the set.

Misalignment imposes an added burden on the

chasers. In addition to cutting the threads, the chasers which are bearing the heaviest on the work are constantly trying to force the turret, or threading spindle, into alignment with the work. When we consider the weight of a threading spindle or turret we can readily appreciate why chaser breakage and other thread troubles may result.



Misalignment may be due to the ways of the machine being worn or may be due to the turret hole not being in line with the work spindle, or it may be due to the turret hole being worn bell mouth allowing the threading tool to drop. A worn die head or one with a bent shank will also cause misalignment.

For checking alignment of the machine, a quick check may be made by bringing the chasers firmly up against the work which, of course, must be true and should be square at the end. Feeler gages or paper can be used in detecting which chasers do not contact the work.

The most accurate method of checking alignment is by mounting an indicator on the spindle of the machine and inserting a plug in the turret hole, the plug projecting six inches, if possible, beyond the face of the turret. See illustration above.

The indicator mounting should be substantial

PROPER SPEED

Threading speed depends on the diameter of the work, the number of threads per inch to be cut and the nature of the material to be threaded. Be sure you are using approximately the correct speed.

The choice of the proper speed for threading is very essential. Many people overlook the importance of this factor, although they use care in selecting the proper speeds for other tooling.

Bear in mind that a threading tool operates on a different principle than most other cutting tools in that the feed per revolution is fixed by the pitch of the thread being cut. This is not so with cutting tools such as those used in turning, forming, etc., where the amount of feed can be varied to suit conditions. Keeping this point in mind, it must be realized that care should be taken in selecting the proper speed.

enough to avoid springing, thus causing an incorrect reading.

By bringing the indicator in contact with the outside of the test bar and rotating the spindle carrying the indicator, errors in concentricity between the spindle and the bar can be noted. The indicator should be set with sufficient spring pressure to counteract the spindle weight when the under side of the test bar is checked.

By setting the indicator so that it contacts the top of the bar and feeding the turret forward and backward, vertical errors in parallelism between the spindle and bar also can be detected. Horizontal errors may be checked in a similar manner on the side of the bar.

In checking for alignment be sure that the turret is in the position where it is used the most — usually the greatest wear is at the forward end.

Too fast a speed will often result in torn threads, burned chasers, rough threads and will, in any case, materially reduce the total life of a set of chasers.

On the following page there is a speed chart of recommended threading speeds showing both F.P.M. (surface feet per minute) and R.P.M. (revolutions per minute). This chart can only be of a general nature and must be altered to suit your own materials and your own working conditions. It will, however, offer a starting point from which you may work in either direction with the idea of obtaining maximum production with best possible finish.

Quite frequently a change in speed downward will result in smooth, shiny threads as opposed to rough, torn threads.

| | Material | Speed Symbol | Material | Speed Symbol | | Material | Speed Symbol | | Material | Speed Symbol | | Suri | ace Spe | ed (F.P . P. I. | '.M.) |
|----------|-------------------------|-----------------|--------------------------|-----------------|------|--------------------|-----------------|------------------------|------------|-----------------|-----------------|------|---------|--------------------|-------|
| z. | Rod | | Celluloid | F | | Carb. | | | Nickel | | Speed Symbol | | 101 1 | . r. i. | |
| ALUMIN. | Cast | F | Copper | E | | 1010-1035 | С | | 2015-2515 | | Symbol | 3 to | 8 to | 16 to | 25 & |
| ∄ | Die Cast | | Everdur | C | | 1112-X1340 | | | Ni-Chrome | | | 71/2 | 15 | 24 | up |
| l | Stamping | | Fibre | F | | Carb. | | | 3115-3450 | _ | | | | | : |
| | Bakelite | | German | E | | 1040-1095 | | | Nitralloy | A | A | 8 | 10 | 15 | 20 |
| | Forging | D | Silver | i | | Mang. | В | ı | Stainless | | | | 10 | 13 | 20 |
| SS | Stamping | E | Wrought | B | | T1330 T1350 | | STEEL | Free Mach. | | В | 15 | 20 | 25 | 30 |
| BRASS | Tubing | | Malleable Cast | C | TEEL | | | $\mathbf{S}\mathbf{I}$ | Stainless | | ь | 15 | 20 | 25 | 30 |
| | Cast | F | Cast | D | E | Chrome | | | (Stringy) | | | | | | |
| | Bar | | Magnesium | F | വ | 5120-52100 | | į | Stamping | B | С | 20 | 30 | 40 | 50 |
| | Naval | D | Monel | A | | Chrome | | | Tool | A | | | | | |
| [-7 | Phosphor | | Metal | | | Van. 6115-6195 | - | | Tubing | В | D | 25 | 40 | 50 | 80 |
| BRONZE | Tubing Cast | | Nickel | D | | | A | | Semi- | D | | | | | |
| <u>@</u> | | E | Rubber | F | | Forging | | | Casting | | E | 40 | 80 | 100 | 150 |
| BH | Bar Mana's | - E | H Bess'm'r | | | Molyb- | | | Zinc | _ | | | | | |
| | Mang'nese Cast Alum. | | Bess'm'r Scr. Stock Cast | С | | denum 4130-4820 | Į | Di | e Casting | F | F | 50 | 100 | 150 | 200 |
| l | Casi Alum. | | ん Cast | | | 7100-4020 | | | | | . ! | | | | |

NOTE: Speeds specified are approximate and may have to be varied to obtain best results.

Table of Speeds

| Surface Speed (F.P.M.) | 8 | 10 | 15 | 20 | 25 | 30 | 40 | 50 | 80 | 100 | 150 | 200 |
|------------------------------|-------|------|------|------|------|-------|------|------|------|------|-------|------|
| Diam. of Work Inches | | | | | | R.P.M | [. | | | | : | l . |
| 1/8 | 245 | 305 | 458 | 611 | 764 | 917 | 1222 | 1528 | 2445 | 3056 | 4584 | 6112 |
| 1/4 | 122 | 153 | 229 | 306 | 382 | 458 | 611 | 764 | 1222 | 1528 | 2292 | 3056 |
| 3/8 | 81.4 | 102 | 153 | 204 | 255 | 306 | 407 | 509 | 815 | 1019 | 1528 | 203 |
| 1/2 | 61.2 | 76.5 | 115 | 153 | 191 | 229 | 306 | 382 | 611 | 764 | 1146 | 152 |
| 5/8 | 48.8 | 61.0 | 91.7 | 122 | 153 | 183 | 244 | 306 | 489 | 611 | 917 | 122 |
| 3/4 | 40.8 | 51.0 | 76.4 | 102 | 127 | 153 | 204 | 255 | 407 | 509 | 764 | 101 |
| 7/8 | 35.0 | 43.6 | 65.5 | 87.3 | 109 | 131 | 175 | 218 | 349 | 437 | 655 | 87 |
| 1 | 30.6 | 38.2 | 57.3 | 76.4 | 95.5 | 115 | 153 | 191 | 306 | 382 | 573 | 76 |
| 11/8 | 27.2 | 33.9 | 50.9 | 67.9 | 84.9 | 102 | 136 | 170 | 272 | 340 | 509 | - 68 |
| 11/4 | 24.4 | 30.5 | 45.8 | 61.1 | 76.4 | 91.7 | 122 | 153 | 244 | 306 | 458 . | 61 |
| 1% | 22.2 | 27.8 | 41.7 | 55.6 | 69.5 | 83.3 | 111 | 139 | 222 | 278 | 417 | 55 |
| 11/2 | 20.4 | 25.4 | 38.2 | 50.9 | 63.7 | 76.4 | 102 | 127 | 204 | 255 | 382 | 51 |
| 15/8 | 18.8 | 23.5 | 35.3 | 47.0 | 58.8 | 70.5 | 94.0 | 118 | 188 | 235 | 353 | 47 |
| 13/4 | 17.4 | 21.8 | 32.7 | 43.7 | 54.6 | 65.5 | 87.3 | 109 | 175 | 218 | 327 | 43 |
| 17/8 | 16.3 | 20.3 | 30.6 | 40.7 | 50.9 | 61.1 | 81.5 | 102 | 163 | 204 | 306 | 40 |
| 2 | 15.3 | 19.1 | 28.7 | 38.2 | 47.7 | 57.3 | 76.4 | 95.5 | 153 | 191 | 287 | 38 |
| 21/8 | 14.4 | 18.0 | 27.0 | 36.0 | 45.0 | 54.0 | 72.0 | 90.0 | 144 | 180 | 270 | 36 |
| 21/4 | 13.6 | 17.0 | 25.5 | 34.0 | 42.4 | 50.9 | 67.9 | 84.9 | 136 | 170 | 255 | 34 |
| 23/8 | 12.9 | 16.1 | 24.1 | 32.2 | 40.3 | 48.3 | 64.4 | 80.5 | 129 | 161 | 242 | 32 |
| 21/2 | 12.2 | 15.3 | 22.9 | 30.6 | 38.2 | 45.8 | 61.1 | 76.4 | 122 | 153 | 229 | 30 |
| 25/8 | 11.6 | 14.5 | 21.7 | 29.0 | 36.3 | 43.5 | 58.0 | 72.5 | 116 | 145 | 218 | 29 |
| 23/4 | 11.1 | 13.9 | 20.8 | 27.8 | 34.7 | 41.7 | 55.6 | 69.5 | 111 | 139 | 208 | 27 |
| 27/8 | 10.5 | 13.2 | 19.8 | 26.4 | 33.0 | 39.6 | 52.8 | 66.0 | 106 | 132 | 198 | 26 |
| 3 | 10.1 | 12.7 | 19.1 | 25.5 | 31.8 | 38.2 | 50.9 | 63.7 | 102 | 127 | 191 | 25 |
| 31/4 | , 9.4 | 11.7 | 17.6 | 23.5 | 29.4 | 35.3 | 47.0 | 58.8 | 94.0 | 118 | 176 | 23 |
| 31/2 | 8.5 | 10.9 | 16.4 | 21.8 | 27.3 | 32.7 | 43.7 | 54.6 | 87.3 | 109 | 164 | 21 |
| 33/4 | 8.1 | 10.2 | 15.3 | 20.4 | 25.5 | 30.6 | 40.7 | 50.9 | 81.5 | 102 | 153 | 20 |
| 4 | 7.6 | 9.5 | 14.3 | 19.1 | 23.9 | 28.7 | 38.2 | 47.7 | 76.4 | 95.5 | 143 | 19 |

For sizes larger than 4" diameter, it is only necessary to bear in mind that speeds change in inverse proportion to the diameter. For example where 3" diameter has 10.1 R.P.M.; 6" diameter would be 5.05 R.P.M. or one half.

GENERAL INSTRUCTIONS

PROPER LUBRICANT

Most materials should be threaded with plenty of lubricant or coolant. Be sure you are equipped with the right one and plenty of it.

We have seen threaded work that has been improved remarkably from the standpoint of finish by changing only one factor — the kind of lubricant employed.

While the general practice is to thread certain materials such as cast brass, cast iron, aluminum, etc., dry, much better results may be obtained through the use of a lubricant or coolant.

When it comes to the threading of alloy steels, steel stampings, steel forgings and other materials in that general classification, success or failure may hinge on the use of the proper lubricant and the amount of lubricant used.

We suggest that with many of these materials a mineral lard oil or oil with a sulphurized base be used. Your oil dealer has done a lot of experimenting with different grades of oil and will be glad to help you pick the proper lubricant or coolant for your work.

The chart below will give you some idea of suggested lubricants, here again these can be only suggestions. The steel stampings you are threading may differ in texture or machinability from those used in some other plant, thus requiring different speeds and lubricants from those used in that other plant on steel stampings (to name only one material as an example).

Furthermore, we cannot emphasize too strongly the necessity of getting a good supply of lubricant to the cutting points of the chasers. Remember the days when you used to brush a little white lead and oil on the chasers? That's very inefficient and very ineffective. Get a good force of high grade lubricant flowing steadily onto your chasers if you value good threads.

Be sure also to use lubricant during any trial cutting, as well as in production.

Above all bear in mind that success or failure in your thread cutting may depend on your choice of lubricant and how you use it. Furthermore, the use of a good quality lubricant is as important as the correct type.

Table of Lubricants and Coolants

| | | | | 10 | eldi | 10 | .ub | rica | ints and Coolants | | | | | | | | |
|------------------------------|--|--|-----------------------|-----------------|----------------------------|----------------------------|--|---|------------------------------|---------------------|-----------------|-----------------------|-----------------|----------------------------|----------------------------|-----------------|-------------------------------------|
| Material | Solution Offi | Dryt | Dry or Soluble Oil | Kerosene Oil | Lard Oil and White Lead | Mineral Lard (20% Lard) | Paraffin Oil | M. N. Lard (20%) or Sulphur Base | Material | Soluble Oil | Dry† | Dry or Soluble Oil | Kerosene Oil | Lard Oil and White Lead | Mineral Lard (20% Lard) | araffin Oil | M. N. Lard (20%) or Sulphur Base |
| Aluminum — Cast | | | | x | | | | | #======== | 101 | 1 | II SI | K | T A | 23 | a, | ≥ 5 |
| Aluminum — Die Cast | | | | x | | | ├─┤ | <u> </u> | Nickel | | | | | | x | | |
| Aluminum — Rod | | | 1 | х | | | | | Rubber | | x | | | | <u> </u> | ┝╼┤ | |
| Aluminum — Stamping | \Box | | | x | | | ├─┤ | | Silver — German | | | | | | | x | |
| Bakelite | | x | | | | | | | Steel — Bessemer | | | | \neg | | x | 1 | |
| Brass — Bar | | T | \vdash | $\neg \uparrow$ | | | x | | Steel — Cast | x | | | _ | | | $\vdash \vdash$ | |
| Brass — Cast | | x | | _ | | | X | | Steel — Carb. Sae 1010-1035 | | | | $\neg \uparrow$ | | x | + | |
| Basss — Forging | | | | - | | | _ | | Steel — Carb. Sae 1112- | | | | _+ | | | -+ | |
| Brass — Navel | | | | + | + | | x | | x1340 | | | | _ | | x | \dashv | |
| Brass — Stamping | | | | -+ | + | | x | | Steel — Carb. Sae 1040-1095 | | | | 十 | | - <u>x</u> | -+ | |
| Brass — Tubing | | 1 | | \dashv | | | | # | Steel — Mang. Sae T1330- | | | _ | _ | | | + | |
| Bronze — Bar | | | | -+ | | | x | # | T1350 | | | | \dashv | | \dashv | \dashv | |
| Bronze — Cast | | x | $\overline{}$ | \dashv | -+ | -+ | <u>x</u> | $-\!$ | Steel — Chrome Sae 5120- | | | | _ | | - | + | |
| Bronze — Cast Aluminum | | 1 | $\overline{}$ | - | | -+ | _+ | # | 52100 | | $\neg \uparrow$ | | - | | | -+ | |
| Bronze — Manganese | | _ | | -+ | | | x | # | Steel — Chrome Van Sae | . – – | | | | | -+ | + | _x_ |
| Bronze — Naval | | \vdash | | + | | + | x | # | 6115-6195 | | | -+ | -+- | + | | + | |
| Bronze — Phosphor | | | | -+- | +- | | X | # | Steel — Forging | | | -+ | ┰ | x | | -+- | _ x _ |
| Bronze — Tubing | | | | | -+ | | x _ | | Steel — Moly. Sae 4130-4820 | | -+- | | + | - | | -+- | |
| Celluloid | | x | | + | | : | X | -43 | Steel — Nickel Sae 2015–2515 | | \dashv | | +- | | | + | × |
| Copper | | | | | | | | | Steel — Ni-chrome Sae 3115- | \neg | _ | | + | -+- | | + | х |
| Everdur | x | - | | \dashv | \dashv | | X L | -#. | 3450 | _ | 十 | + | + | - | | + | |
| Fibre | | x | | +- | | | + | | Steel — Nitralloy | _ | + | - | + | \dashv | $-\!\!\!\!+$ | | × |
| Iron — Cast | | | | -+- | | | + | _ 5 | Steel — Stainless | \neg | | -+- | + | \dashv | | +- | x |
| Iron — Malleable | x | -+ | X | -+- | | | 4 | - 5 | Steel — Stamping | | | -+ | + | -+ | | +- | x |
| Iron — Wrought | X | | -+ | -+- | | | 4 | | Steel — Tool | -+- | +- | | +- | | | 4 | X |
| Magnesium | + | | | -+- | -+- | | | S | Steel — Tubing | | +- | -+- | +- | \dashv | x | + | |
| Monel Metal | +-+ | -+ | - - | X . | | - | \bot | S | teel — Semi Casting | x | +- | -+- | +- | | | ┿ | X |
| | ·] | ! | 1 | ĺ | : | K | | Z | inc - Dio Co-ti | $\frac{\hat{x}}{x}$ | + | | +- | | - | +- | _ |
| † Usually run dry but we rea | | | | | | | | | | ~ | t | 1 | 1 | 1 | | 1 | 1 |

[†] Usually run dry but we recommend a coolant.

THREADING TROUBLES

'Threading Trouble' usually means that something is causing production of unsatisfactory threads on the work piece. The chart shows common thread defects and the possible causes.

The remedies, if not self evident, can be found by following the suggestions for proper operation as covered in the various sections of this book.

Experience has proved that a vast majority of threading troubles can be traced to the conditions under which the work is being done and not to original faults in the tools. It is even possible that a setup which works perfectly on one type of material will not be satisfactory for another type. So do not be too quick to lay the blame for threading troubles on the tools, check the entire setup including the material being threaded.

It will be noted that any given 'symptom' might be caused by any one of a number of conditions and possibly by a combination of several.

| | | | |] | EFFECT | | | · · · · · · · · · · · · · · · · · · · |
|------------------------|------------------------|------------------|--------------------|--------------------------------|---|---------|---------------|---------------------------------------|
| . Cause | Poor Thread Form | Rough Threads | Tapered Threads | Stripped or Torn Threads | Chattered- out of Round- Drunken Threads | Shaving | Lead Error | Incorrect Pitch Diameter |
| CHASERS | | | | | | | | |
| Incorrect Chamfer | x | x | x | x | x | x | x | |
| Incorrect Face Grind | x | х | x | х | х | x | х | х |
| Incorrect Bearing | ж | x | x | x | х | ж | | |
| Incorrect Clearance | | | x | | | x | | |
| Too Keen | x | | x | | х | х | x | x |
| Dull | x | x | x | | | | x | |
| Worn Keyways | x | | x | | | х | | |
| DIE HEAD | | | | | | | | |
| Worn Parts | x | | x | x | | x | | x |
| Misalignment | x | | х | х | | x | x | |
| MACHINE | | | | | | | | |
| Improper Camming | x | | x | | | x | × | |
| Incorrect Speed | ж | x | х | х | x | x | x | |
| Inexperienced Operator | · x | | x | х | | x | × | |
| LUBRICATION | | | | | | | | |
| Wrong Kind | | x | | x | | | 1 | |
| Insufficient | х | х | | x | | | | |
| SHAVING | х | | х | x | | | х | х |

OPERATING SUGGESTIONS

Before starting to cut a thread check chasers carefully. If threading to a shoulder or bottom, be sure the chasers have a short enough chamfer for the work. If it is not to a shoulder, do the chasers have a long enough chamfer to do the best possible job? The longer the chamfer the easier the chasers will cut and the better thread they will produce. See chart of commonly used chamfer angles on page 30.

Also be sure chasers have correct face grind for the nature of the material to be threaded. See chart of recommended face grinds on page 33.

Do not run the die head up on the work without checking the diameter of work or adjustment of die head. A piece of work oversize or die head adjusted too small will cause chasers to remove excess stock, which is very likely to cause chaser breakage.

Make a sample cut, after which finer adjustments may be required to fit gages.

When shoulder threading, allow extra clearance to avoid running into the shoulder. Finer adjustment can then be made for proper length of thread.

Help feed the turret along while threading, following lead of the screw, thus avoid having the die head pull the entire slide along. Avoid putting too much pressure on, forcing the turret; likewise avoid holding back on turret causing a drag. Advance the turret at the same rate as the lead of the thread being cut. Learn feel of the machine for different thread leads.

Be sure to use lubricant during any trial cutting, as well as in production.

Take good care of your tools when in use, and when not in use. Keep them clean and do not abuse them by driving them into or out of the turret. This may spring the head and throw it out of alignment.

Clean chips and dust out of it regularly. Periodically take apart, remove old gummy oil, oil the working parts and put it together again. When not in use, put in a dry place with a rust preventive brushed on.

If these rules are followed carefully, there will be less chance of Die Head troubles or chaser breakage and better threads will be cut.



SELF OPENING

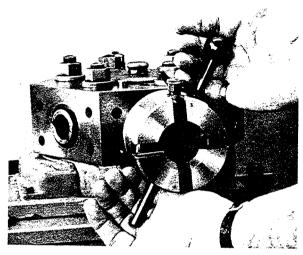
Setting up for operation

1. TRIPPING INTO OPEN POSITION

Normally the Die Head has been installed in the turret or spindle of the machine before the chasers are inserted. The first step in chaser insertion (or removal) is to trip the head into open position.

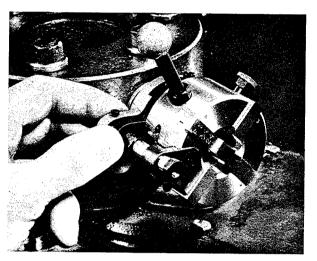
If the chasers were in the head this is the position where chasers are disengaged from the work.

Each style of Geometric Die Head is tripped in a different manner as described below.



STYLES D AND C (PULL OFF ONLY)

Pull the front part of the die head toward you by means of the closing handle until the head unlocks, allowing the cam to rotate into open position.



STYLES DS, DSA AND DD

Push back trip lever and cam will rotate into open position.



STYLES KD, KDS, CK

Push back on trip flange, causing head to trip into open position.

2. OPENING FOR CHASER INSERTION

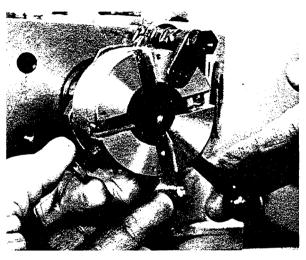
This is the *fully* open position and differs from the ''open'' position described on the opposite page in that the chaser slots are now ''opened'' or cleared of the mechanism that holds the chasers in place.

The various methods of clearing the slots for chaser insertion for the different styles of Die Heads are shown below.



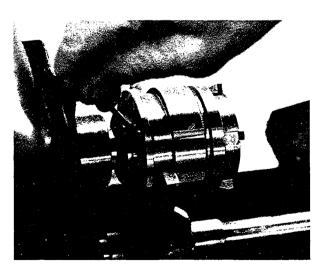
STYLES D, DD, C, CT

Relieve the pressure of the cam spring by lightly pushing on handle. At same time pull up stop plunger and the cam will rotate into fully open position.



STYLES DS, DSA

Relieve the pressure of the cam spring by lightly pushing on closing handle or pin. At same time pull up stop plunger and the cam will rotate into fully open position.



STYLES KD, KDS, CK

Depress stop lever in adjusting ring with your thumb or with some implement, allowing the springs to force back the closing sleeve into open position.



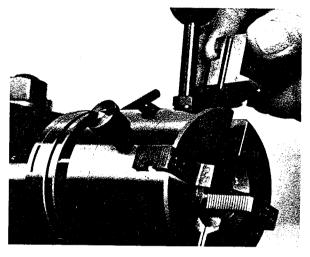
SELF OPENING

Setting up for operation

3. INSERTING CHASERS

The chaser slots on each Die Head are stamped in sequence 1, 2, 3, etc. Individual chasers in a set are also marked in this manner. It is important that each chaser be inserted in the slot with the corresponding number. So, when inserting chasers in the die head,

put the chaser stamped No. 1 in the slot stamped No. 1, chaser stamped No. 2 in the slot stamped No. 2, and so on. Be sure D type chasers are positioned properly. With K chasers the pin in the bottom of the chaser should snap into the chaser spring plunger.

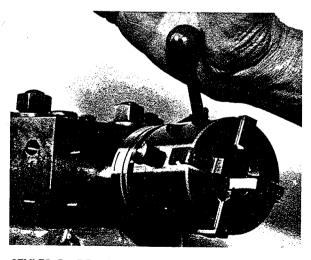


STYLES D, DD, C, CT, DS, and DSA

Push the D type chasers in until the push button snaps into the lug slot.

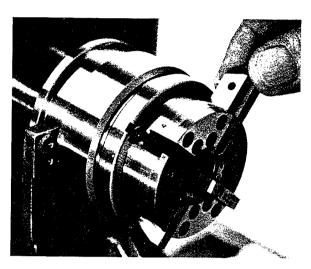


With the chasers in the die head, close the tool so that the chasers are in cutting position, that is, with the tool completely closed and the chasers in position



STYLES D, DD, C, CT and DS

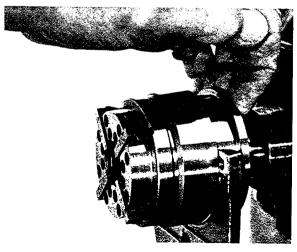
Rotate cam by means of closing handle, being sure to continue rotation after the stop plunger snaps into position, and until head locks in cutting position.



STYLES KD, KDS and CK

Push the K type chasers in until the chaser pins in chasers are firmly held in the spring plungers. This can be determined by a slight click as each chaser seats properly.

to cut a thread. This will lock the chasers in place so that they may not be removed until the head is again fully opened as described on page 13.

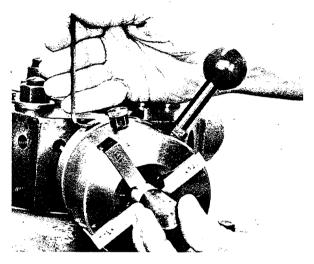


STYLES KD, KDS and CK

Pull the trip flange forward, being sure to continue the forward motion after the stop lever snaps into locking position and until head locks into cutting position (on KH2 use closing handle).

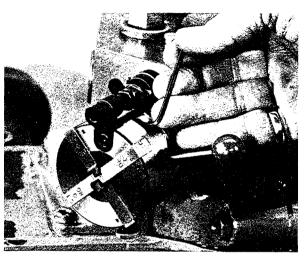
5. ADJUSTING CHASERS TO SIZE

If a sample screw is available adjust the chasers to this part. If not, use as a setting gage a piece of bar stock turned to the minor (root) diameter of the thread to be cut. Care should be taken not to force the chasers into the setting gage. The adjusting of the chasers to size varies with the type of die head employed. Illustrated below are the methods employed with some of the more commonly used types of Geometric Die Heads.



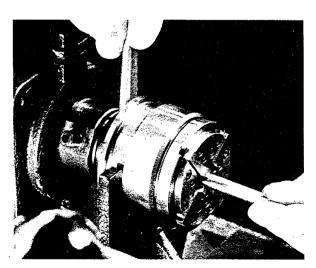
STYLES D, DD

Adjust to cutting size by loosening one adjusting screw and tightening the other. A hex key is provided for this purpose.



STYLES DS, DSA

Adjust to cutting size by loosening one adjusting screw and tightening the other. A hex key is provided for this purpose.



STYLES KD, KDS, CK

Loosen the adjusting ring binding screw using the hex key provided. Then by means of a pin inserted in the hole of the adjusting ring turn until the desired thread size is obtained. Tighten adjusting ring binding screw before cutting a thread.



SELF OPENING

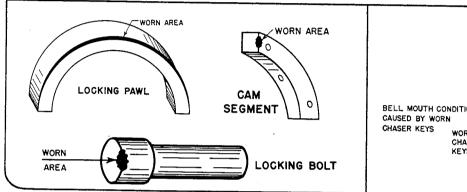
6. REPLACEMENT OF PARTS

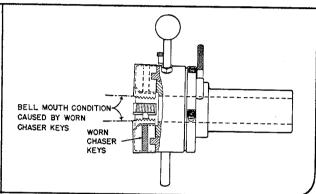
Geometric tools as a rule are noted for their simplicity of construction and freedom from mechanical faults. However, as it may be necessary occasionally to replace worn or damaged parts, a few general instructions on parts replacement will be helpful. Should you care for information on any problem of this sort that is not covered in this book, our engineers will be glad to answer specific questions at any time.

Most die heads use a number of coil springs. Check these springs now and then to be sure they have their original flexibility. If springs are used in pairs, be sure they are of equal size and strength. Another point to check frequently is the locking medium. Whether this be a locking bolt or pawl the continual opening and closing of the tool are bound to cause wear on these essential parts. They should be renewed from time to time.

Needless to say, that part of the die head in which the chasers are located is of prime importance. The chaser slots should not show material wear nor should the chaser keys or other holding devices be permitted to wear materially without replacement.

Detailed construction of the more common tools and list of parts are shown on pages 17-25.





Style D Die Head

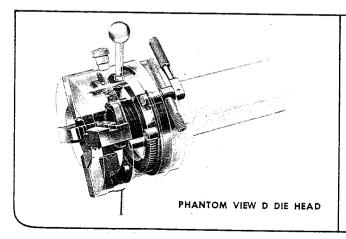
The removal of the thimble, back in the bore from the face of the tool, is necessary in order to entirely disassemble this type of tool. A broad nose screw driver will do this easily and quickly.

The cam spring may have to be replaced occasionally. After putting the die head in a vise, remove the front part of the head by unscrewing the thimble. Then take out the cam spring plate screws, allowing the cam spring plate and cam spring to be removed.

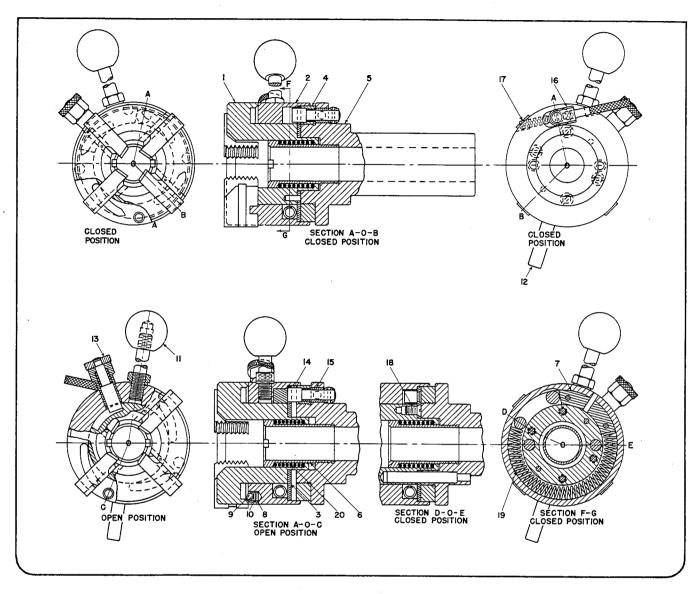
To reassemble tools $1\frac{1}{2}$ " in size or smaller, first replace the cam spring plate and cam, then insert the new cam spring from the lug side of the cam.

On sizes larger than $1\frac{1}{2}$ place the cam in a vise

with the lugs down, holding on the lugs lightly so cam cannot turn. Insert cam spring in the cam spring chamber placing one end of the spring against the segment, with the other end of spring projecting slightly. Place the cam spring plate in position so the cam spring stop pin will pick up the end of the cam spring that is projecting. Next, rotate the cam spring plate sufficiently to allow the cam spring stop pin to drop into position. Remove this unit from the vise holding the cam and cam spring plate together so the cam spring cannot release itself. This unit can now be placed on the die head skeleton and the cam spring plate screws inserted.



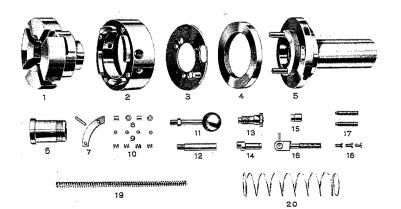




PARTS FOR DIE HEAD - STYLE D

WHEN ORDERING REPAIR PARTS GIVE BOTH NUMBER AND NAME OF PART AND SERIAL NUMBER OF TOOL.

- 1—Skeleton with chaser keys and cam spring plate pins.
- 2—Cam with push buttons, rings and springs.
- 3—Cam spring plate with cam spring stop pin.
- 4-Adjusting ring.
- 5—Back part with driving pins (specify shank size when ordering).
- 6-Thimble.
- 7—Cam segment with pins.



- 8—Push button rings.
- 9-Push buttons.
- 10—Push button springs.
- 11—Closing handle, assembled.
- 12—Closing pin.
- 13—Stop plunger complete.
- 14—Locking bolt.
- 15-Locking bolt bushing.
- 16-R&F Lever with pin.
- 17—Adjusting screws.
- 18—Cam spring plate screws.
- 19—Cam spring.
- 20—Thimble spring.

DECEMPS

SELF OPENING

6. REPLACEMENT PARTS — CONTINUED

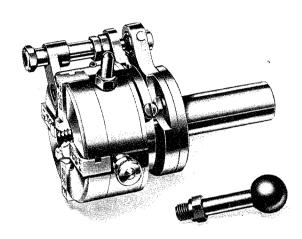
DISASSEMBLY

Style DS Die Head

With die head in open position and chasers and tripping mechanism removed, place face down on

bench and remove the two tapered head cam spring

plate screws from the rear of the die head. On some die heads to get access to the cam spring plate screws it is necessary to disassemble the shank by removing the two square head screws. however most die heads have screw driver clearance holds through shank flange. When removing the cam spring plate screws hold the die head with the fingers so the parts will not release too quickly due to pressure of springs.



Remove the cam spring plate and backpart assembly, being very careful to hold parts together so the cam spring will not fly out. Now the two units, one the cam spring plate-back part assembly and the other the skeleton-cam assembly can be taken apart.

To disassemble skeleton-cam assembly, hold the skeleton in one hand and with the fingers of the other hand pull up the stop plunger and remove the cam.

The die head is now completely disassembled with the exception of a few parts which need no explanation.

To disassemble cam spring plate-back part assembly, it is necessary to remove shank then place the cam spring plate-back part assembly back in skeleton assembly less cam, buffer pins and springs, and cam spring. Now block up the back part near the driving pins

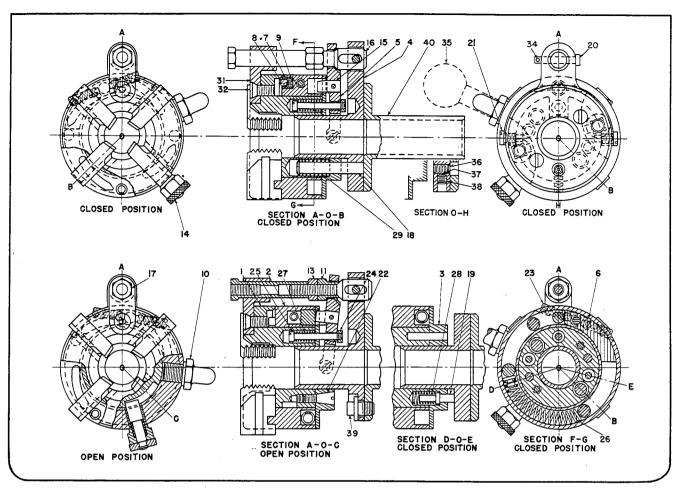
so there will be space between the cam spring plate and back part. Place the entire unit face down on the bench and knock out the driving pins from the rear with a hammer and punch. This will release the two major parts.

ASSEMBLY

First, put the back part on the bench with the pilot facing upward. Place the cam spring plate over the pilot of back part with the hole in the trip lever in line with the trip screw hole in the back part and line up the driving pin holes between the two parts. Put springs on the driving pins and insert the small end of the pins through the cam spring plate and into the back part, using a hammer and punch to finally drive pins into position. Drive pins into position so that the ends of the driving pins will be SLIGHTLY UNDER the rear surface of the back part. Now place back partcam spring plate assembly in the vise, holding from the flange and in a horizontal position. Place the two buffer pins in the holes in the cam spring plate, with the large end of the buffer pins in the cam spring plate. Next place the two buffer springs over the buffer pins. Assemble cam to skeleton and rotate cam until stop plunger drops into recess. Now hold skeleton-cam assembly face down on the bench and insert the cam spring. When inserting the cam spring, position the cam so that the segment is toward you, then place the cam spring in the chamber and compress spring against the pin to the left, allowing the opposite end

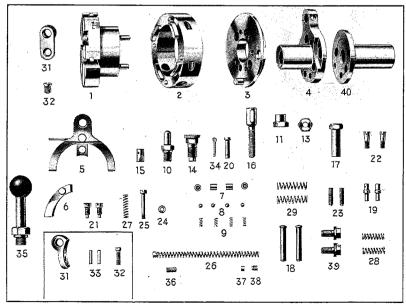
of the spring and shoe to project slightly out of the chamber when against opposite pin. This shoe prevents spring from catching in final assembly.

Now assemble skeleton-cam assembly to back part-cam spring plate assembly as follows: — With the back part-cam spring plate assembly in vise, place the skeleton-cam assembly on the back part-cam spring plate assembly, lining up the spring and pin holes. Next, compress the two units together and when doing so pull out the stop plunger in the cam, allowing cam to rotate slightly lining up the cam spring stop pin in the cam with the one in the plate. Then rotate the cam and pick up the end of the cam spring that is projecting. By rotating the cam in this manner the cam spring stop pin in the cam spring plate will drop into position in the cam spring chamber and by additional pressure the two units can be brought together. Holding the two units together, remove entire assembly from vise and place face down on bench still holding parts in place. Now insert the two cam spring plate screws from the rear and tighten in position. Shank can now be assembled lining up clearance hole through flange with buffer action lock out screw. Reassemble tripping mechanism.



PARTS FOR DIE HEAD - STYLE DS

WHEN ORDERING REPAIR PARTS, GIVE BOTH NUMBER AND NAME OF PART AS WELL AS CONSTRUCTION NUMBER AND SERIAL NUMBER OF TOOL.



- —Skeleton with chaser keys and cam spring plate pins
- Cam with push buttons, rings, springs and cam spring stop pin
- *3—Cam spring plate with cam spring stop pin
- 4-Back part
- 5—Trip lever with locking bolt pin
- 6—Cam segment with pin
- 7-Push button rings
- 8-Push buttons
- 9-Push button springs
- 10—Closing pin
- 11—Tripping nut
- 13-Outside trip gage lock nut
- 14-Stop plunger complete
- 15-Locking bolt
- 16-Trip screw
- 17—Outside trip gage
- 18-Driving pins
- 19—Buffer pins
- 20-Trip screw pivot pin
- **21—Yoke lever pivot { Screws

- 22-Cam spring plate screws
- 23-Adjusting screws
- 24-Trip lever screw nut
- 25-Trip lever screw
- 26-Cam spring
- 27 -- Trip lever spring
- 28 Buffer springs
- 29 Return springs
- †31 Outside trip gage bracket
- †32—Outside trip gage bracket screw
- 33—Outside trip gage bracket pins
- 34--Trip screw pivot cotter pin
- 35-Closing handle
- 36 Buffer action lock out screw
- 37—Buffer action lock out binding screw shoe
- 38-Buffer action lock out binding screw
- 39—Aligning shank screws
- 40—Shank—Specify shank size when ordering

*Parts 1 and 3 ground together. They should be ordered together wherever possible, to insure interchangeability.
**On the 5/16", 9/16" and 3/4" DS, the pivots are screws. In 1" and larger DS heads, the pivots are pins.

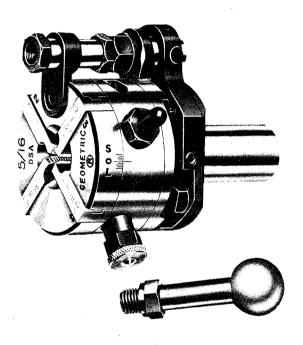
†Parts No. 31 and 32 are used in 9/16" and larger sizes. The parts shown in the box at the lower left are used in 5/16" size only.

Construction of the 1-1/4'' DS is somewhat different from the other sizes. If difficulty in determining the correct parts for this size is encountered, the order should be accompanied by a complete description or a sketch of the part desired. NOTE: part desired.

Parts 4 and 40 are integral in sizes 1-1/4" and 1-3/4".

SELF OPENING

6. REPLACEMENT PARTS — CONTINUED Style DSA Die Head



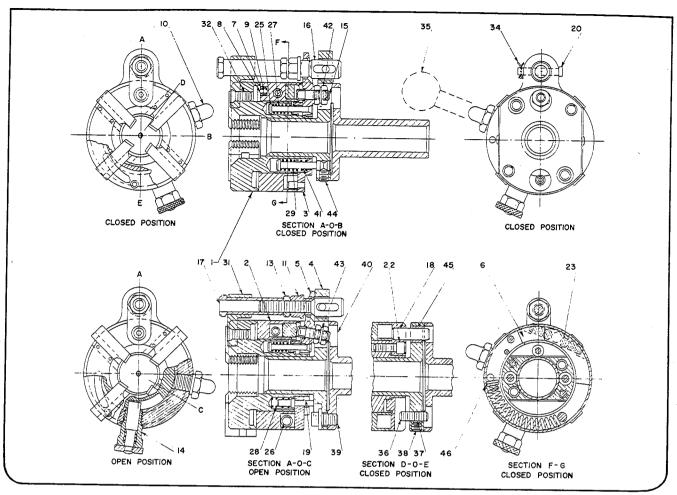
DISASSEMBLY

Remove chasers and tripping mechanism and with the die head in open position, loosen the two return spring pin binding screws on the flatted sides of the backpart. Loosen these screws until a slight click is heard but do not remove them completely. The front portion of the die head can now be removed from the backpart and shank. Using another size hex key remove the cam spring plate screws from the back of the front portion of die head. Remove the cam spring plate assembly being careful to prevent the cam spring from coming out. To disassemble skeleton and cam pull out on stop plunger in case it is engaged. Other smaller parts can be easily disassembled.

ASSEMBLY

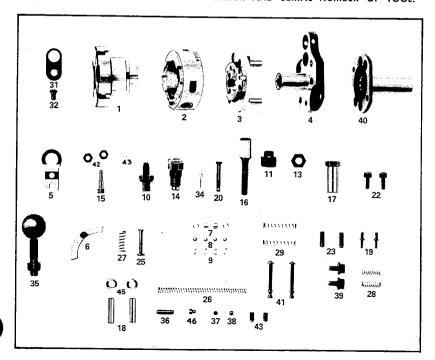
Install cam spring in cam between pins with the shoe end of cam spring toward the two pins in cam. Assemble cam and skeleton. Assemble trip lever spring and spring pin in trip lever slot in cam spring

plate. Next compress trip lever spring so trip lever can be inserted and the head of pin inserted in trip lever. Place return springs on return spring pins and assemble to cam spring plate working from inside bore. The cam spring plate assembly can now be assembled to the cam and skeleton by inserting the return spring and trip lever springs in proper holes. The cam should be rotated on the skeleton so that the cam spring stop pin in the cam spring plate can be inserted in the space provided between the shoe on the cam spring and the stop pin in the cam. Cam spring plate screws can now be inserted and tightened. Now cam can be rotated on skeleton until locking bolt is engaged and the front portion of die head assembled to the backpart and shank. Care should be taken to get the return spring pins in holes and compress the buffer action before tightening the two return pin binding screws. Assemble tripping mechanism and die head is ready for use.



PARTS FOR DIE HEAD - STYLE DSA

WHEN ORDERING REPAIR PARTS, GIVE BOTH NUMBER AND NAME OF PART AS WELL AS CONSTRUCTION NUMBER AND SERIAL NUMBER OF TOOL.



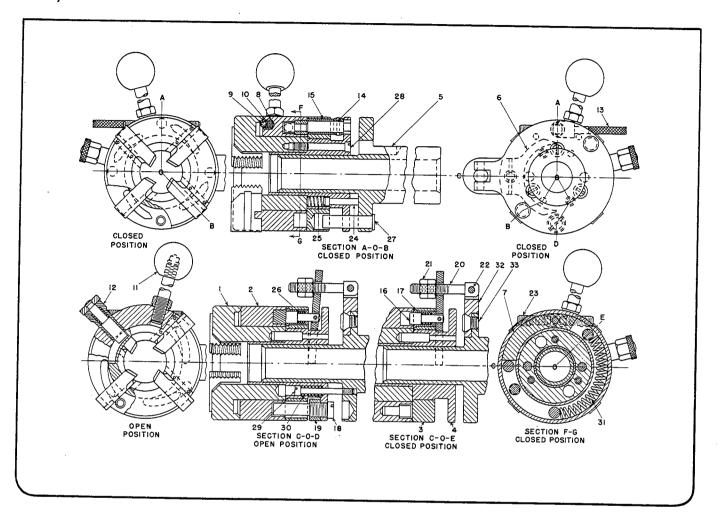
- 1. Skeleton with chaser keys
- 2. Cam with push buttons, rings, springs and cam spring stop pins
- Cam spring plate with cam spring stop pin and driving pins
- 4. Back part and driving pin bushings
- 5. Trip lever
- 6. Cam segment with pin
- 7. Push button rings (6*)
- 8. Push buttons (6*)
- 9. Push button springs (6*)
- 10. Closing pin
- 11. Tripping nut
- 13. Outside trip gage lock nut
- 14. Stop plunger complete
- 15. Locking bolt
- 16. Trip screw
- 17. Outside trip gage
- 18. Driving pins
- 19. Buffer pins
- 20. Trip screw pivot pin
- 22. Cam spring plate screws (4*)
- 23. Adjusting screws

- 25. Trip lever pin
- 26. Cam spring
- 27. Trip lever spring
- 28. Buffer springs
- 29. Return springs
- 31. Outside trip gage bracket
- 32. Outside trip gage bracket
- 34. Trip screw pivot cotter pin
- 35. Closing handle complete
- 36. Buffer action lock out screw
- 37. Buffer action lock out binding screw shoe
- 38. Buffer action lock out binding screw
- 39. Aligning shank screws (3*)
- 40. Shank—Specify shank size when ordering
- 41. Return spring pins
- 42. Locking bolt nuts
- 43. Locking bolt lock washer
- 44. Return spring pin binding
- 45. Driving pin bushing
- 46. Cam spring shoe
- *Number of parts required in $2\frac{1}{4}$ " DSA Die Head



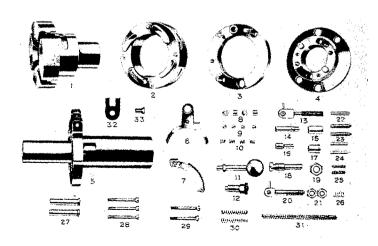
6. REPLACEMENT PARTS - CONTINUED Styles DD and C

Style DD



PARTS FOR DIE HEAD - STYLE DD

WHEN ORDERING REPAIR PARTS, GIVE BOTH NUMBER AND NAME OF PART AS WELL AS CONSTRUCTION NUMBER AND SERIAL NUMBER OF TOOL



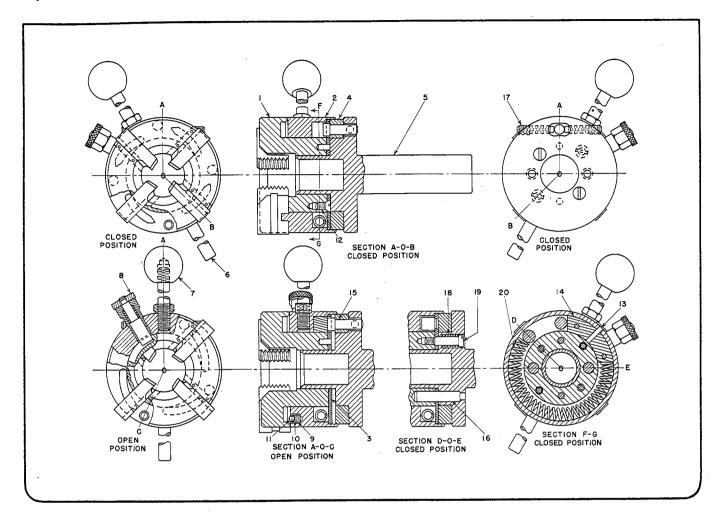
- 1—Skeleton with chaser keys. 15—R&F eccentric bushing.
- Cam with push buttons, 16—Locking bolt. rings, springs, and cam spring stop pins.
- -Back part ring with locking bolt bushing, eccentric bushing and lever stop
- 4-Back part with back part 21-Trip screw nuts. pins.
- *5—Shank (specify shank size 23—Adjusting screws.
- Trip lever with locking bolt 24—Buffer pins. pin.
- 7—Cam segment with pin.
- 8-Push button rings.
- 9-Push buttons.
- 10—Push button springs.
- 11—Closing handle, assembled. 30—Return springs.
- 12—Stop plunger complete.
- 14-R&F eccentric.
- 13-R&F lever with pin.

- 17—Locking bolt bushing.
- 18-Cam spring stop screw.
- 19—Cam spring stop screw nut.
- 20-Trip screw with pin.
- 22—Trip screw pivot pin.

- 25—Buffer springs.
- 26-Locking bolt spring. 27—Driving pins.
- 28-Back part screws.
- 29—Return spring screws.
- 31—Cam spring.
- 32—Trip screw head
- 33-Trip screw head screw.

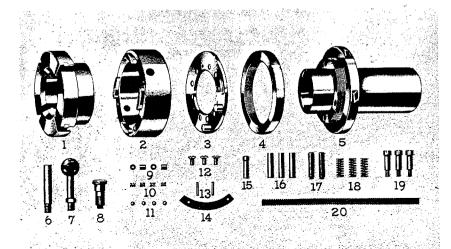
*Used with Style DD hand type only.

Style C-Pull-Off Trip Type



PARTS FOR DIE HEAD - STYLE C - Pull-Off Trip Type

WHEN ORDERING REPAIR PARTS, GIVE BOTH NUMBER AND NAME OF PART AS WELL AS CONSTRUCTION NUMBER AND SERIAL NUMBER OF TOOL.



- 1—Skeleton with Chaser Keys and Cam Spring Plate Pins.
- 2—Cam with Push Buttons, Rings and Springs.
- 3—Cam Spring Plate with Cam Spring Stop Pins.
- 4—Adjusting Ring.
- 5-Back Part (specify shank size when ordering).
- 6—Closing Pin.
- 7—Closing Handle.
- 8-Stop Plunger Complete.
- 9-Push Button Rings.
- 10—Push Button Springs.
- 11—Push Buttons.
- 12—Cam Spring Plate Screws.
- 13-Cam Segment Pins.
- 14—Cam Segment.
- 15-Locking Bolt.
- 16—Driving Pins.
- 17—Adjusting Screws.
- 18-Return Springs.
- 19—Return Spring Screws.
- 20—Cam Spring.

NOTE—Some "C" Heads are arranged with Roughing and Finishing Attachments. In this case the Locking Bolt No. 15 has an eccentric end. The extra parts are the Locking Bolt Bushing and Roughing and Finishing Lever with Pin—not shown in illustration.

DIE ZEADS W

SELF OPENING

6. REPLACEMENT PARTS — CONTINUED Styles KD and CK Die Heads

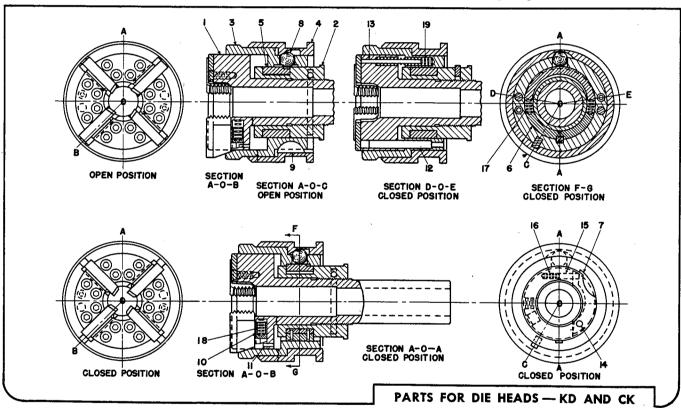
No tools, except a small hex key, are necessary for disassembly of the KD and CK Die Heads. With the head closed, release the screw in the adjusting ring.

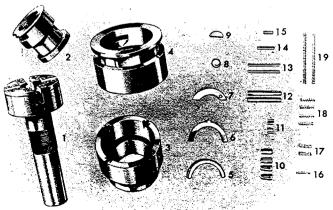
Then unscrew the adjusting ring from the shank of the skeleton, now pull the skeleton forward from the assembled trip flange, closing sleeve and adjusting ring. With your thumbs pushing forward against the closing sleeve, reach inside the assembly and release the adjusting ring by pushing it backward and out with your fingers. When disassembling the closing sleeve and trip flange care should be taken to prevent the ball dropping out. See sectional view below. To reassemble, replace pawl and segment in groove of adjusting ring, being sure the broader face of the

pawl is toward the narrower rim of the groove.

Keep the pawl springs under tension as you replace the adjusting ring.

Be careful to line up the springs in the closing sleeve with the corresponding holes in the skeleton; keep the closing sleeve forward while screwing the adjusting ring on to the skeleton. Then tighten the set screw in the adjusting ring.





WHEN ORDERING REPAIR PARTS GIVE BOTH NUMBER AND NAME OF PART, ALSO CONSTRUCTION NUMBER AND SERIAL NUMBER OF TOOL.

| 1—Skeleton with front | 3—Closing Sleeve. Clos- | |
|---|--------------------------------------|------------|
| plates and front plate screws. Skeleton As- | ing Sleeve Assembly includes Closing | 12 |
| sembly also includes 2 | Sleeve Guide Pins. | 12- |
| Closing Sleeve Spring | 4-Trip Flange. | 13- |
| Pins. 2—Adjusting Ring with | 5—Pawl. | |
| binding shoe and set | 6—Segment with Key. 7—Stop Lever. | 14 15 |
| screw. Adjusting Ring | 8—Ball. | 19 |
| Assembly also includes | 9-Woodruff Key. | 16- |
| Stop Lever, Stop Lever Pivot Pin, Stop Lever | 10—Chaser Spring Plungers. | 17- 18- |
| Spring Pin and Stop * | 11—Chaser Spring | 19- |
| Lever Spring. | • | |

| IOWDEK OF IO | OL. |
|-----------------------------------|---|
| g Sleeve. Clos- leeve Assembly | Plunger Retaining Pins. |
| des Closing | 12—Closing Sleeve |
| o Guide Pins. | Guide Pins. |
| lange. | 13—Closing Sleeve |
| ent with Key. Lever. | Spring Pins. 14—Stop Lever Pivot Pin 15—Stop Lever Spring Pin. |
| ruff Key. or Spring | 16—Stop Lever Spring. 17—Pawl Springs. |
| ers. | 18—Chaser Springs. |
| r Spring | 19—Closing Sleeve |
| | Springs. |

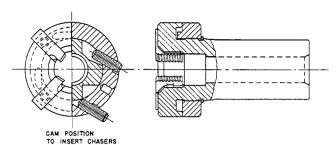
*Screws with Lock Washers replace these pins on 1" size Die Head and larger.

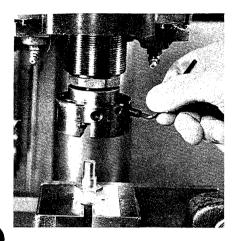
IMPORTANT NOTE: The construction of the Style KD and the Style CK is identical with the following exceptions: The 2½" and 3½" CK have two pawls (Part No. 5); no segment (Part No. 6); the adjusting ring (Part No. 2) is shorter in length; they also have one additional part (not shown) known as a skeleton ring.

SOLID ADJUSTABLE

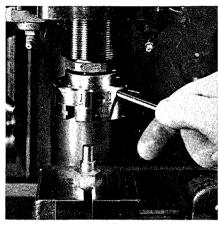
Style DJ

Everything that has been said about the operating conditions and care of Self Opening Die Heads on the foregoing pages is equally applicable to Solid Adjustable Die Heads. However, not having the self opening mechanism they are much simpler in construction. There are just two major parts — the Skeleton which holds Chasers in place, and a Cam which acts as both a locking and size adjustment medium.

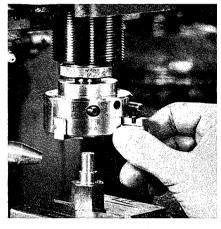




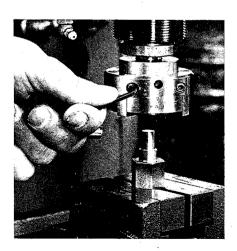
 Before inserting or removing chasers, first back out the adjusting screw shown in illustration.



Insert a pin in the hole on the periphery of the Cam and revolve the Cam on the Skeleton toward the left.



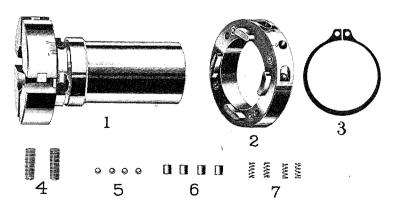
3. The Chasers, which are held in by Push Buttons, can then be taken out (or inserted) with the fingers. Insert Chaser No. 1 in slot No. 1, No. 2 in slot No. 2, and so on.



4. Adjust to cutting size loosening one adjusting screw and tightening another. Set to a slightly larger diameter than you intend to cut. Then, adjust in the small direction until the desired size is obtained. In this way backlash is eliminated.

PARTS FOR DIE HEAD — STYLE DJ

WHEN ORDERING REPAIR PARTS, GIVE BOTH NUMBER AND NAME OF PART PLUS SIZE, CONSTRUCTION NUMBER AND SERIAL NUMBER OF THE DIE HEAD.



- 1. Skeleton with Chaser Keys. (Specify Shank size.)
- 2. Cam with Push Buttons, Rings, and Springs.
- 3. Cam Retaining Ring.
 Older models and present 6" Head have Cam
 Retaining Keys and Key Screws instead of Ring.
- 4. Adjusting Screws.
- 5. Push Buttons.
- 6. Push Button Rings.
- 7. Push Button Springs.

DIE HEAD CHASERS

| Chamfer Angles 30 |
|-----------------------|
| Ground (Milled) 28 |
| Milled 28 |
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| Breakage 42 |
| Keen, Too 40 |
| Lead Error 41 |
| Shaving 41 |
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| Cutting Face 32–33 |
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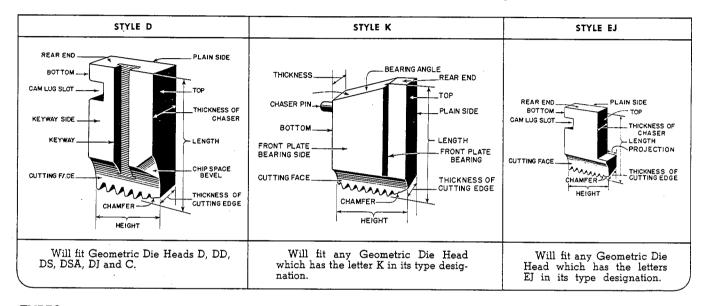
die head chasers

STYLES

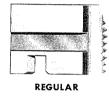
Die Heads of any type would be useless without cutters. These cutters are called CHASERS and the fact that they are adjustable is what gives to Die Heads their great advantage over solid dies. Chasers usually come in sets of four but a set may consist of more depending on the size of the Die Head.

Since the correct operation of your Die Heads will depend largely on the performance of the Chasers, we cannot emphasize too strongly the importance of top quality chasers to begin with, and the utmost care in selecting the correct chaser for the job in hand.

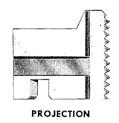
To equip all types of Geometric Die Heads, there are three chaser styles as illustrated below



TYPES



Chasers are also classified as "Regular" or "Projection." The projection type, as the name implies, project out beyond the face of the Die Head when in place. This is not only an advantage when threading close to a shoulder but because of the longer threaded section they permit of a larger number of rechamferings.



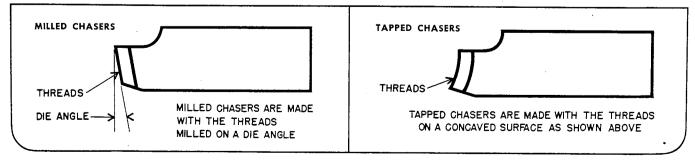
For the general run of work under ordinary conditions.

For close to shoulder threading.

TAPPED VS "MILLED" CHASERS

In addition to classification by Style and Type, Die Head chasers may also be classified by conformation of the thread profile, i.e., "Milled" and "Tapped."

These two terms may, however, be misleading as by custom they refer to the shape and not necessarily, as the names imply, to the manner in which the threads were generated. In other words, ''Milled'' refers to a straight die angle no matter how it was generated, whether milled or ground, and ''Tapped'' merely indicates a concave profile.



TERMS RELATING TO CHASERS

BEARING This is the surface in contact between the chaser and the work BEARING SHOWN when cutting the thread. AT SHADED PORTION CIRCUMFERENTIAL CLEARANCE CUTTING FACE (Tapped Form and S Chasers) To provide relief circumferentially between chaser and work as shown so that the chaser will contact the work at the cutting face only. CIRCUMFERENTIAL CLEARANCE DIE ANGLE CUTTING FACE (Milled, Ground thread or Tapped Form Chasers) Relief between the chaser and the work is provided by the Die Angle, i.e., the angle at which threads are milled. DIE ANGLE TOP LONGITUDINAL CLEARANCE (Milled, Ground thread or Tapped Form Chasers) To provide clearance longitudinally between the chaser and work as shown so all of the cutting will be LONGITUDINAL CLEARANCE воттом done at the chamfer. MOVE (Single Thread) The distance or advance of a given thread from chaser to chaser TOP is the "MOVE." The distance is the same from one chaser to the next in a set (on single thread). TRACKAGE Chasers "track" properly when all chasers of a set follow exactly in the groove cut by the preceding chaser or chasers. (See move). CUTTING **SHAVING** Shaving is the side cutting action of one or more chasers resulting in thin threads. For further information see page 37. SHAVING ON FRONT SHAVING ON REAR SIDE OF TEETH SIDE OF TEETH



Before starting to cut a thread there are several fundamental things that should be checked.

First of all, examine the blueprint of the work to be produced and make certain you have the proper tools for the work. Check especially carefully the chasers furnished. The chasers can make all the difference between success or failure on a threading job.

The chamfer (often called throat or lead) of a chaser is the beveled portion which leads the tool onto the work. As the cutting is all done by the chamfer and first full tooth back of the chamfer, it is important that the chamfers be right for the job.

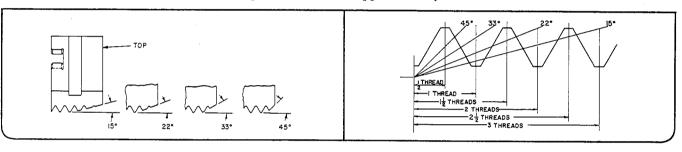
CHAMFER ANGLES

The correct chamfer angle depends on the type of work to be threaded. For shoulder threading 45° is usually employed. For straightaway threading a 22° chamfer is standard. On tough alloy steels a longer chamfer should be used where permissible.

If you are threading to a shoulder or bottom, be sure the chasers have a short enough chamfer for the work. If it is not to a shoulder, do the chasers have a long enough chamfer to enable them to do the best possible job? The longer the chamfer the better the distribution of chips. This means easier cutting, better finish on the work and longer chaser life.

Chasers should also have the correct face grind for the material to be threaded. In fact incorrect face grind will result in more trouble than any other one factor in threading. It is very important to distinguish between chamfer grinding and face grinding.

The figures in the chart are based on American National or V threads. On Acme, Worm, Modified Square and similar thread forms, a two-thread chamfer is approximately 15°, a one-thread chamfer approximately 33°.



SHARPENING CHASERS

Nothing contributes more to the production of accurate threads, and low cost per thread, than accurate sharpening of chasers. Frequent light grinding or touching up will not only give better threads but will greatly extend the life of the chasers. Partial dullness leads to chipping as well as poor threads.

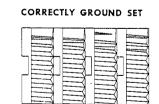
Chamfer Grinding

One point which should be stressed is the necessity of resharpening chasers at the chamfer. On milled chasers, in fact, practically all resharpening should be done at the chamfer with the cutting face only

Therefore, to obtain the best results from any chasers they should be resharpened frequently and before they become dull. They should be resharpened by machine using an appropriate grinding fixture. They should not be resharpened free hand. See pages 34-35 for sharpening fixtures.

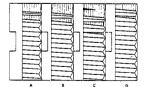
touched up lightly from time to time as needed.

For quick recognition of correct and incorrect chamfers, a few are illustrated here.



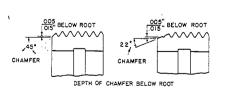
Note that chamfer is slightly different on each chaser of set. For explanation see illustration of ''Move'' on page 29.

INCORRECTLY GROUND SET



Chaser B is correctly ground. Chaser C has been ground with too long a chamfer. Chaser D has too short a chamfer. Also Chaser A is too thin and not of the same thickness as the other three chasers of the set.

DEPTH OF CHAMFER



The chamfer should start .005" to .015" below the root of the chaser teeth. All chasers of a set should be ground at uniform angle and depth so that each chaser will start cutting at the same time.

Chamfer Grinding (Cont.)

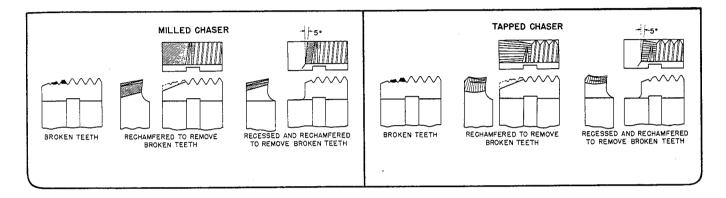
RECESSING AND RECHAMFERING

For shoulder threading where a long chamfer is not permissible, it is frequently necessary to recess the front face of the chasers to remove dull, worn or chipped teeth. The chasers must then be rechamfered with a one thread chamfer, which is the minimum recommended for shoulder threading.

Incidentally, this same method of recessing is used when only long chamfer chasers are available and you want to use them for shoulder threading. Here again the chasers must be rechamfered after recessing.

All chasers must be recessed uniformly, with 5° rake.

When projection chasers are employed, grind back the projection sufficiently to remove any worn or chipped teeth. Be sure that chasers for shoulder threading have a 5° rake ground on top so that they will have only a single point contact with the work in case of accidentally hitting shoulder. Projection chasers must be rechamfered after grinding back the projection.



CHAMFER CLEARANCE

In sharpening chasers, not only must the chasers have correct angle of chamfer but they must also have the proper chamfer clearance.

Too much chamfer clearance will cause chattered threads, tapered threads and poor lead. Reverse chamfer clearance will prevent the chasers from cutting freely and perhaps result in broken chasers.

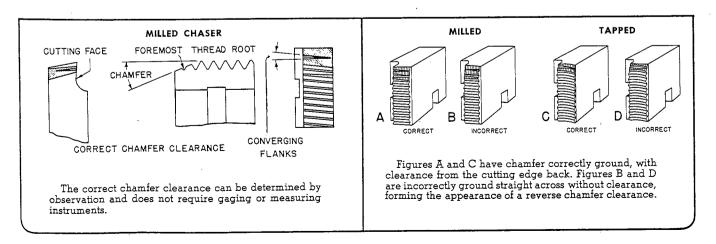
In setting up the chasers for rechamfering, first select the chaser of a set having the foremost thread root at the chamfer.

Second, set up the chaser in a fixture so that in grinding, the flanks of the chamfered teeth will converge as shown, thus indicating that the chamfer has

proper clearance.

It is good practice to observe the amount of clearance on the chaser before regrinding so it can be duplicated readily.

The amount of clearance is, to a certain extent, dependent upon the nature of material being threaded. The amount of clearance on the chamfer of the milled type of chaser is approximately ½° to 1° more than the die angle measured on the helix of the chaser. For tapped chasers, clearance should be slightly more than the circumferential clearance. When threading aluminum the amount of clearance should be double that for other materials.



SHARPENING CHASERS (Continued)

Grinding Cutting Face

On the preceding pages we have stressed the importance of grinding chasers, especially milled chasers, principally at the chamfer.

However, chasers must also be resharpened occasionally on the cutting face. With milled chasers rechamfer first. Should the cutting edges show dullness, then touch up the cutting face lightly, removing only .002" to .003".

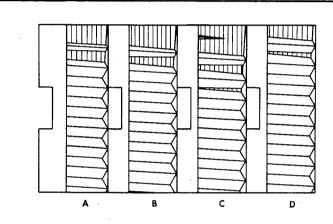
Tapped chasers can be resharpened on the cutting face much more freely. When threading to a shoulder with tapped chasers it is usual to do most of the resharpening on the cutting face but they should be rechamfered if the chamfered teeth are badly worn.

It is important that the width of the land or thickness

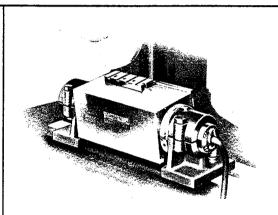
of cutting edge should be uniform on all chasers of a set or the load of cutting will be thrown entirely upon the thicker chaser or chasers, resulting in unsatisfactory threads.

Never grind chasers free hand. Always use a grinding fixture or grind them on a surface grinder equipped with a suitable work holder. The usual procedure is to employ a magnetic chuck on a surface grinder thus enabling you to resharpen all chasers of a set at one set-up. This, of course, insures equal resharpening of all chasers.

Before setting up, be sure you know what face grind should be employed. Use the chart on the opposite page as a guide.



Result of uneven grinding. Cutting edge A is thinner than others. Chamfer is also incorrect.

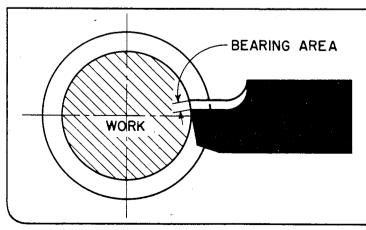


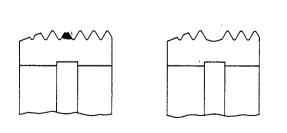
Grinding a complete set of chasers on a surface grinder with magnetic chuck.

The illustration shows how milled chasers contact the work. Note the "Bearing Area." As soon as this area is removed by grinding back the cutting face, chasers will chatter. Therefore it is important that the cutting face of milled chasers be ground only lightly — a few thousandths of an inch

at any one resharpening.

Sometimes a tooth here or there is broken. Often these broken teeth may be ground out. Care should be taken not to disturb flanks of teeth adjoining the broken tooth.





REMOVING BROKEN TOOTH BY GRINDING

CHASER FACE GRINDING CHART

DIE HEAD CHASERS — ALL STYLES

RIGHT HAND CHASERS — Use this Chart.

LEFT HAND CHASERS — Use this Chart.

TAPER DIE HEAD CHASERS

Use same Grind as for Straight Thread Chasers.

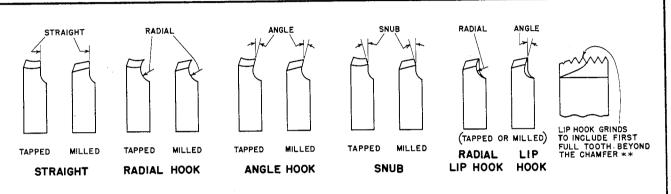
MULTIPLE THREAD MILLED CHASERS

Instructions furnished with each set of Chasers.

ALL OTHER DIE HEAD CHASERS

Instructions furnished upon request.

The Cutting Face Grinds specified are approximate and due to conditions may have to be varied to obtain best results.



**Lip Hook Grinds not recommended for Shoulder or Bottoming Work, in this case use the same angle but omit the lip.

| | Milled Form and | l Tapped Form | M + 1.1 | Milled Form and | d Tapped Form |
|---|--|--|--|---|---|
| Material | Straight Thread | Taper Thread | Material | Straight Thread | Taper Thread |
| Aluminum — Die Cast Aluminum — Rod Aluminum — Stamping Bakelite Brass — Bar | 15° Radial Hook 15° Radial Hook 15° Radial Hook 15° Radial Hook 5° Snub 5° Hook 5° Snub 10° Hook | 10° Radial Hook 10° Radial Hook 10° Radial Hook 10° Radial Hook 5° Snub Straight 5° Snub 5° Hook | Monel Metal Nickel Rubber Silver — German Steel — Bessmr. Scr. Stock Steel — Cast Steel — Carb. SAE 1010-1035 Steel — Carb. SAE 1112-X1340 Steel — Carb. SAE 1040-1095 Steel — Mang. SAE T1330-T1350 Steel — Chrome SAE 5120-52100 Steel — Chrome Van. SAE 6115-6195 Steel — Forging Steel — Molybdenum SAE 4130-4820 Steel — Nickel SAE 2015-2515 Steel — Ni-Chrome SAE 3115-3450 | 15° Radial Hook 10° Hook 15° Hook 5° Snub 10° Hook 10° Hook 10° Hook 10° Hook 10° Hook 15° Hook | 10° Radial Hook 5° Hook 10° Hook 5° Snub 5° Hook 5° Hook 5° Hook 5° Hook 10° Hook |



RESHARPENING FIXTURES

The accuracy of finished threads is largely dependent upon the precision with which chasers are chamfered. Uneven chamfers throw the cutting on one or two chasers of a set. That means lead errors, taper threads, poor threads.

You can't get uniform and accurate chamfers by grinding free hand. They can, however, be easily achieved with the chaser grinding fixtures described on this and the opposite page.

Should the Style A Fixture be used with \%6'' DS, \%6'' K Chasers or \%6'' EJ5 Chasers, special Holders as shown in Figure 3 are required. The Holder shown can be used for the \%6'' DS or the \%6'' K. (The Chasers located on the key with the \%6'' DS; forced against the key with the \%6'' K.) Still another holder of similar design is required with \%6'' EJ5 Chasers. None of these special Holders are included with the Style A Fixture but must be purchased at a slight additional Cost.

Style A Fixture

Milled, Ground and Supermetric Die Head Chasers, may be rechamfered with the Geometric Style A Chamfer Grinding Fixture.

The graduations permit setting the Fixture Table to desired angle of chamfer clearance.

Both right and left hand chasers can be rechamfered — the Table being tilted down for right hand chasers, and up for left hand chasers.

Figure 1 is a side view of Style A Fixture. An adjustable stop governs the position of the chaser in respect to the grinding wheel.

The adjustable stop has ends of varying height. Use low end whenever possible. This adjustable stop must contact the teeth at back end of chaser. In operation the key in the top of the Fixture engages the keyway in D type chasers and acts as a guide while grinding. Clearance should be allowed between the adjustable stop and the bottom of D type chasers.

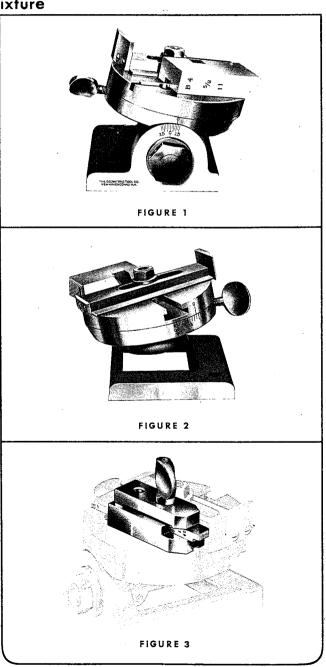
With K type chasers the bottom of chaser should be located against that side of the adjustable stop which has been milled out for clearance for the chaser pin. Clearance should be allowed between the key and front plate bearing of K chasers.

Figure 2 is Style A Fixture from the opposite side. The graduations permit swiveling the Fixture Table to desired angle of chamfer. Both short and long chamfers may be produced by setting table the desired angle, i.e., 45°, 33°, 22°, and 15°.

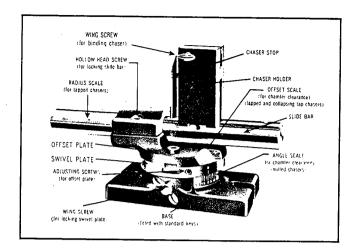
To use the Fixture, first set at the proper chamfer clearance angle. (See Fig. 1.) Lock in place by means of hexagon nut. Next swivel the table to desired chamfer angle locking the table in place by means of thumb screw. The Fixture is, of course, securely fastened to the table of the grinding machine.

The usual grinding procedure is shown in Fig. 3. The chaser is fed forward by hand against the side of the wheel until it contacts the adjustable stop. Grind the other members of the set at the same setting to insure uniformity of chamfer.

It is possible to feed the machine table forward in which case the chaser is held firmly against the adjustable stop on the Fixture, the table being fed forward to a stop arranged on the machine.



GEOMETRIC STYLE "E" UNIVERSAL CHASER GRINDING FIXTURE

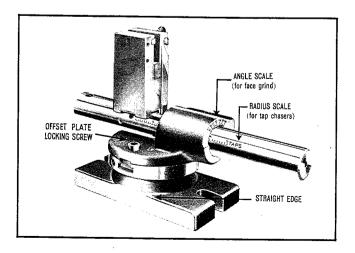


Here's a Universal Fixture that's inexpensive, simple and compact, yet one which, while designed primarily for grinding all types of Chasers on the chamfer, can also be used for grinding the cutting face. Milled, Ground and Supermetric Chasers with a flat chamfer, Tapped Chasers with a concave chamfer, Collapsing Tap Chasers with a convex chamfer, all may be easily and quickly reground by making a few changes in the set-up of the Fixture and Holders. Both Right and Left Hand Chasers may be sharpened with equal ease.

special features

The Style E Fixture can be used with most universal grinding machines.

A Swivel Plate permits the Chaser Holder to be offset to give the proper chamfer clearance to Tapped (Hobbed) Chasers or Collapsing Tap Chasers. This plate is equipped with Opposed Adjusting Screws for providing fine adjustment which may be readily made and then locked solidly in place, thus permitting the easy duplication of grinds. The tongue and groove method of locating the Chaser Holder on the Slide Bar gives an accurate location and sturdy support.



a complete unit The Fixture is a complete unit in itself. One Chaser Holder for one tool size of Geometric Chaser is furnished with every Fixture at no additional cost. Additional Chaser Holders for Geometric Chasers can be obtained at a nominal charge. (See page 38.) For grinding other makes of Chasers, blank Chaser Holders can be furnished which can readily be altered by the user.

simple to use It is a very simple matter to use this Fixture. It is easy to set for the distinct type of Chaser you wish to sharpen, being equipped with readily visible scale readings and when once set, all the Chasers of the set can be uniformly reground without again altering the set-up.

need not be an expert One of the big advantages of this Fixture is that any mechanic can quickly and easily set up the Fixture and adjust it, thus making unnecessary the employment of a special grinding expert.

all chasers should be sharpened To obtain the best results from any Chasers they should be sharpened frequently and before they become dull. If accuracy and production per set of Chasers are desirable, then the Chasers must be ground accurately on both the cutting face and chamfer. (Milled, Ground and Supermetric Chasers, however, must be ground only lightly on the cutting face. (See pages 32 & 37.) Unequal grinding of the Chasers in a set causes the Chasers to cut unevenly and poor threading results are inevitable. Chasers should never be ground by hand.

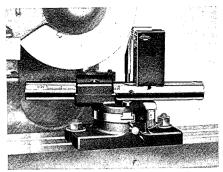
uniform grinding We have just pointed out the dangers of hand grinding, or machine grinding not uniformly done. With the Geometric Universal Grinding Fixture, once the Fixture is adjusted all the Chasers in a set are bound to be uniformly reground.

INSTRUCTIONS FOR USE chamfering milled, ground and supermetric chasers

- (1) With the Radius Scale marked "Dies", the Base Scale "B" Fig. 1, and the Slide Bar Locking Screw all facing toward you insert Slide Bar into fixture.
- (2) Clamp the suitable Chaser Holder in position as Shown in Fig. 1, using the inner screw hole in the Slide Bar with the head of Wing Screw in Holder toward you. Insert the Chaser Stop at the left of the Holder.
- (3) Set the Slide Bar so that its center line (at "A" Fig. 1) is at zero and lock it tightly. (Radius Scale not used for Milled, Ground and Supermetric Chasers.)
- (4) Insert the Chaser with chamfer up in the Holder, bringing the threaded end against the Chaser Stop and lock in position by means of the Wing Screw in Chaser Holder. "D" Type Chasers should be located



on the Key provided in the Chaser Holder. The Keys are reversed in the Holders when grinding 5/16" and 9/16" "K" Type Chasers and removed entirely for all larger sizes of "K" Chasers. To



Figure

follow or duplicate the original grind as to chamfer, adjust the Machine until the contact between the periphery of the Grinding Wheel and chamfer will produce the desired angle of chamfer.

- (5) The Swivel Plate should now be set to an angle (See B, Fig. 1) which will coincide with the original chamfer clearance angle of the Chaser, and locked in place by means of the Wing Screw (See C, Fig. 1). Be sure Offset Plate Locking Screws (See D, Fig. 1) are tight before any grinding is done. (No Offset Plate adjustment required for Milled, Ground and Supermetric Chasers.)
- (6) Feed the Chaser forward carefully against the Grinding Wheel by means provided on the Machine and at the same time pass the Chaser back and forth across the periphery of the Wheel, grinding very lightly to see that the chamfer clearance is correct. A Stop on the Machine, or other suitable means, should be provided so that all Chasers of the set will be ground an equal amount.

chamfering tapped die head chasers

- (1) With the Radius Scale marked "Dies", the Base Scale "B" Fig. 1, and the Slide Bar Locking Screw all facing toward you insert the Slide Bar into fixture. (See Fig. 2.)
- (2) Clamp the suitable Chaser Holder in position as shown in Fig. 2, using the inner screw hole in the Slide Bar with the head of Wing Screw in Holder toward you. Insert the Chaser Stop at the left of the Holder.
- (3) Set the Slide Bar so that the reading on the Radius Scale marked "Dies" (A, Fig. 2) will equal as nearly as possible half of the minor (root) diameter of the thread. See page 69 for method of figuring minor diameter.
- (4) Set the Slide Bar so that its center line (At "E" Fig. 2) is at zero and lock it tightly.

- (5) Insert the Chaser with chamfer up in the Holder, bringing the threaded end against the Chaser Stop and lock in position by means of the Wing Screw in Chaser Holder. "D" Type Chasers should be located on the Key provided in the Chaser Holder. The Keys are reversed in the Holders when grinding 9/16" "K" Type Chasers and removed entirely for all larger sizes of "K" Chasers.
- (6) To follow original grind as to chamfer, adjust the Machine until the contact between the periphery of Grinding Wheel and chamfer will produce the desired angle of chamfer. (See Fig. 2.)
- (7) Loosen two Offset Plate Locking Screws (At "B" Fig. 2) and adjust Offset Plate by means of Adjusting Screws (See C, Fig. 2) to proper amount (use Scale at D, Fig. 2) to provide for proper clearance on chamfer. With the Slide Bar as shown in Fig. 2 the direction of offset should be away from you for Right Hand Chasers, and towards you for Left Hand Chasers. If figures are unavailable judge amount of offset by original clearance on Chasers being reground. Once having obtained correct chamfer clearance, lock Offset Plate in position by means of Offset Plate Locking Screws (See B, Fig. 2).
- (8) Feed the Chasers forward carefully against the Grinding Wheel by means provided on the Machine and at the same time rock the Chaser back and forth across the peri-

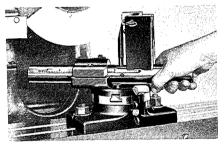


Figure 2

phery of the Wheel, grinding very lightly to see that the chamfer clearance is correct. A Stop, or other suitable means, should be provided on the Machine so that all Chasers of the set will be ground an equal amount. The width of the Wheel at the periphery must be thin enough so that it is suitable for the radius on the Chaser.

chamfering collapsing tap chasers

- (1) Insert the Slide Bar with the Radius Scale marked "Taps" and Base Scale (B, Fig. 1) towards you and with the Slide Bar Locking Screw away from you. (See Fig. 3.)
- (2) Clamp the suitable Chaser Holder in position as shown in Fig. 3, using the Inner Screw Hole in the Slide Bar with the head of Wing Screw in Holder away from you.
- (3) The Chaser Stop is not used with Holders for "S" Chasers for 1" to 2" tap sizes inclusive, nor with Holder for $\frac{3}{4}$ " "SL" Chasers. Set the Chasers firmly

against the Angle Plate in the Holder. The Angle Plate must be set so the threaded portion of the Chaser is vertical and to the left. When using these Chaser Holders the reading on the Radius Scale marked "Taps" (See C, Fig. 3) should always be set at $\frac{7}{8}$ ". When this is done set the Slide Bar so that its center line is at zero and lock it tightly.

(4) For Chasers larger than 2" Tap size insert the Chaser Stop at the left of Holder (no Angle Plate in Holder being required). Insert the Chaser with the chamfer up in the Holder bringing the threaded end

against the Chaser Stop and lock in position by means of the Wing Screw in Chaser Holders With these Chaser Holders the Slide Bar should be set so that the reading on it will equal

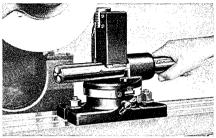


Figure 3

as nearly as possible half of the major (outside) diameter of the thread. When this is done set the Slide Bar so that its center line is at zero and lock it tightly.

- (5) To follow the original grind as to chamfer adjust the Machine until the contact between the periphery of the Grinding Wheel and chamfer will produce the desired angle. (See Fig. 3.)
- (6) Loosen two Offset Plate Locking Screws (At B, Fig. 3) and adjust Offset Plate (use Scale—See D, Fig. 2) by means of Adjusting Screws (one shown at D, Fig. 3) so that original chamfer clearance may be maintained. With Slide Bar parallel to the Wheel as shown in Fig. 3 the direction of offset should be away from you for Right Hand Chasers and towards you for Left Hand Chasers. If figures are unavailable, judge amount of offset by original clearance on Chasers being reground. Once having obtained correct chamfer clearance, lock Offset Plate in place by means of Offset Plate Locking Screws (See B, Fig. 3).
- (7) Feed the Chaser forward carefully against the Grinding Wheel by means provided on the Machine and at the same time rock the Chaser back and forth across the periphery of the Wheel, grinding very lightly to see that the chamfer clearance is correct. A Stop, or other suitable means, should be provided on the Machine so that all Chasers of the set will be ground an equal amount.

chamfer angle setting gage

A simple device used for setting the grinder to the desired angle of chamfer on any of the Chasers heretofore mentioned is a Setting Gage that can be obtained at a slight additional charge.

Set Gage to desired angle of chamfer. Clamp Chaser in Chaser Holder and place the Setting Gage on

top of Chaser with the swivel end towards periphery

of Grinding Wheel. Adjust the Machine until both points of swivel end of Setting Gage contact the wheel. Be sure Grinding Wheel is not in motion.



CUTTING FACE GRINDS

It is quicker and more convenient to grind a complete set of Chasers at a time on the cutting face, making use of a magnetic chuck tilted to the desired angle. The Style "E" Fixture, however, can be used for face grinding if desired, even though it is primarily only a Chamfer Grinding Fixture.

grinding the cutting face of die head chasers

Chasers used in Holders for ¾ "size Die Head Chasers or smaller, are ground with the Holders mounted in a vertical position as shown in Fig. 4. Reverse the Key Plate (B, Fig. 4) in the Chaser Holder, if necessary, so that the Chaser can be clamped with the thread up as illustrated. Set the Slide Bar so that straight, snubbed

or hooked cutting face can be ground as desired. Graduations are provided for this purpose. (See A, Fig. 4.) Feed the Chaser against the side of the wheel by means provided on the

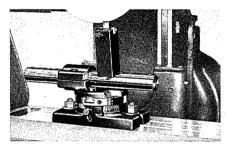


Figure 4

Machine, passing it back and forth as it is being ground.

Chasers used in Holders for Die Head Chasers sizes larger than $\frac{3}{4}$ " are ground with the Chaser Holders mounted in a horizontal position as shown in Fig. 5. It is necessary to use the Key in these Holders for "D" Chasers, but it must be removed for "K" Chasers. Fasten Stop Plate (B, Fig. 5) to Holders to suit Right or Left Hand Chasers. Set the Slide Bar so that straight, snubbed or hooked cutting face can

be ground as desired. Graduations are provided for this purpose. (See A, Fig. 5.) Insert the Chasers in the Holder bringing the threaded end against the Stop Plate. Feed the Chaser against

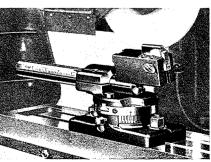


Figure 5

the side of the Wheel by means provided on the Machine, passing it back and forth as it is being ground. A Stop, or other suitable means, should be provided on the Machine so that all Chasers of a set will be ground an equal amount.

Milled, Ground and Supermetric Chasers should be ground principally on the chamfer, but can be touched very lightly on the cutting face occasionally.

grinding the cutting face of collapsing tap

Chasers used in Holders up to and including 2" Tap size are ground with the Chaser Holders mounted in a vertical position as shown in Fig. 6. Set the Angle Plate in the Chaser Holder so that the Chaser can be clamped with the threads horizontal as illustrated. Set

the Slide Bar so that straight, snubbed or hooked cutting face can be ground as desired. Graduations are provided for this (See A, Fig. 6.) Feed the Chasef against the side of the Wheel by means provided

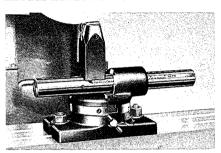


Figure 6

on the Machine, passing it back and forth as it is being ground. A Stop, or other suitable means, should be provided on the Machine so that all Chasers of the set will be ground an equal amount.

Chasers used in Holders larger than 2" Tap size are ground with the Chaser Holders mounted in a horizontal position as shown in Fig. 7. Fasten the Stop Plate (See B, Fig. 5) to Chaser Holder to suit Right or Left Hand Chasers. Set the Slide Bar so that straight, snubbed or hooked cutting face can be ground as desired. Graduations are provided for this purpose.

(See A, Fig. 7.) Insert the Chaser in the Holder, bringing the threaded end against the Stop Plate. Feed the Chaser against the side of the Wheel by means provided on the Machine, passing it back and

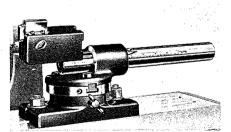


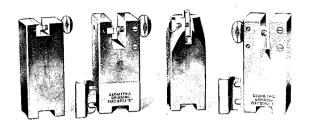
Figure 7

forth as it is being ground. A Stop, or other suitable means, should be provided on the Machine so that all Chasers of the set will be ground an equal amount.

specifications

The Geometric Universal Chaser Grinding Fixture is furnished complete, together with only one Chaser Holder, at list price. In placing orders be sure to specify the Chaser Holder you require, as well as any additional Holders which may be necessary and which are furnished at additional cost.

CHASER HOLDERS



A separate Chaser Holder is required for each different size of chaser blank. Avoid mistakes by ordering by Chaser Holder number (see list below). The illustration above shows the four general types of Holders. Holders for 5%'' to 34" Die Head Chasers inclusive. Note Removable Plate with Key.

Holders for 1" and larger Die Head Chasers. Note Removable Kev.

Holders for 34" to 2" Tap Chasers inclusive. Note Adjustable Angle Plate.

Holders for 21/2" and larger Tap Chasers.

At the left of the second and fourth Holders is shown the Stop Plate for face grinding not used in chamfering.

Specify Chaser Holders by number and avoid mistakes.
(*Regarding Special Short Holders see page 39)

| Holder Number | Used With | Holder Number | Used With |
|---------------------------------|---|---|---|
| 2 3 4 5 6 7 8 | %6" DS and %6" K %6" D and %6" K %2" D "D and 1" K 1.4" D and 1 K 1.4" D and 1 K 1.4" D and 1 K Chasers for Tools 1.4" Or larger 1.4" D 2" and 2 ½" D | 9 10 11 12 13 14 15 16 24 25 | 3", 3½" and 4½" D 1"S 1¼"S 1½"S 2"S 2"S 4" and 4½" S 5" and 6"S ½"S 5" sel 6"S ½" SL5 |

The Style "E" Fixture is not suitable for Tangemetric and Circometric Chasers. The Style F fixture should be used.

recommended chamfers

A long chamfer should be used on all Chasers wherever it is possible to do so. While a 2-thread chamfer is usually satisfactory, on certain tough materials a 3-thread, or even longer chamfer, will give better results. A short, 1-thread chamfer, is usually used where the thread is cut close to a shoulder, but even under such circumstances it is often possible to use a 1½ thread chamfer. Remember that the longer the chamfer the less will be the stress thrown on the first full tooth of the Chasers.

Approximate Angle of Chamfer in Relation to Threads

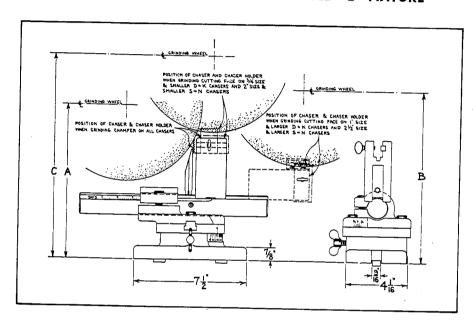
| Number of | Angle of Char | nfer |
|----------------------|---|-------------------------------------|
| Threads Chamfered | Amer. Nat'l (U.S.), V, Whitworth, Metric Thread Forms | Acme and Similar Thread Forms |
| 1 | 45° | 33° |
| 1 1/2 | 33° | 22° |
| 2 | 22° | 15° |
| 3 | 15° | |

In designing the Style "E" Grinding Fixture, we had to keep in mind the necessity of re-sharpening all Geometric Chasers from the 3%" EJ5 to the 3%" D, from the 3%" SL to the 6" S. Thus the Fixture had to be large enough and high enough to give proper clear-

ances for re-sharpening all these types of Chasers.

*SPECIAL SHORT HOLDERS—When clearances on machine will not permit the regular Holders to be used, contact us regarding possibility of using shorter Holders.

PRINCIPAL SPECIFICATIONS OF STYLE "E" FIXTURE



To determine if the Style "E" Fixture can be adapted to a Grinding Machine, consult the following tables, which give the clearance needed for the type of Chasers being sharpened, and the angle of chamfer desired.

| | WHE | ЕБ РС | SITIO DI | N FOR MENS | GRIN | IDING A"* | CHAI | MFER | | | | | WHEEL POSITION CUTTIN | | | NING |
|---------------------------------------|--------|----------|-----------------------|---------------|---------|--------------|--------|--------|--------|--------|--------|---------|--------------------------|-------------|-------------|-------------|
| | 1 | 5° Cha | mfer | 2 | 2° Cha | mfer | 3 | 3° Cha | mfer | 45 | ° Char | nfer | DIMENS | ION "B | ,,, | |
| Size and Type | v | Vheel I | Diam. | | Wheel 1 | Diam. | W | heel I | Diam. | w | heel D | .am. | Size and Type Chasers | 6" | 8" | 10′′ |
| Chasers | 6′′ | 8′′ | 10" | 6" | 8′′ | 10′′ | 6" | 8′′ | 10" | 6′′ | 8" | 10" | 1" & Larger-D & K | AA Ueel | Wheel | Whe |
| %6″ EJ5 | 85/8′′ | 87/8" | 1 | 9′′ | 93/8" | 93/4" | 91/2" | 10" | 101/2" | 10" | 10%" | 113/8′′ | 2½" & Larger-S | 91/4" | 1014" | 111/4 |
| %6" to 1½"-K %6"-DS & %6" to 1½"-D | 9′′ | 91/4" | Interferes Fixture | 93/8′′ | 9¾″ | 101/8" | 91/8" | 10¾" | 11" | 103/81 | 11" | 1134" | DIMENS | ION "C | ″ | |
| 1" to 2"-S 2" and 2½"-D | | 91/2" | Wheel I | 95%" | 10" | 103/8" | 10%4 | 10567 | 1114" | 10560 | 111/// | 10" | Size and Type Chasers | 6" Wheel | 8" Wheel | 10" Whee |
| 2½″ to 3½″-S | | | | | | | 10% | 1072 | 1174 | 1078 | 11 74 | 12. | 3/6" EJ5 | 111/4" | 121/4" | 131/4 |
| %/′′-SL` | 9½″ | 9¾" | 10" | 91/8" | 101/4" | 10%″ | 103/8″ | 10%″ | 111/2" | 10%" | 111/2" | 12¼″ | -5/6"-DS and K | 111/2" | 121/2" | 131/21 |
| 4″ to 6″-S | 9¾″ | 10" | 1014" | 101/8′′ | 101/2" | 10%" | 10%″ | 111/4" | 11¾″ | 111/8" | 113/8" | 12½" | 1" to 2"-S | /- | -2/1 | 13/2 |
| 3" and 3½"-D | 101/2" | 103/8′′′ | 10%" | 10½″ | 10%" | 111/4" | 11" | 11½″ | 121/8" | 11½″ | 12¼″ | 121/8" | %6" and %"-D %6"-K | 11%" | 12¾" | 13¾′ |

^{*}Dimensions given are for Regular Chasers. For Projection or Overhanging Chasers Add Amount of Projection or Overhang to Dimension "A"



Servicing

INCORRECT BEARING

If chasers have too heavy bearing they will rub too hard producing taper or rough threads or causing chaser breakage. Milled form chasers may be corrected by grinding the cutting face by .002'' to .003'' increments.

When there is not enough bearing, the chasers should be lapped to provide more.

For lapping a mixture of fine emery and oil is applied before engaging the teeth. Note in Fig. 1 below that the teeth at chamfer ends are fully engaged. Rear teeth do no cutting so no harm is done if not lapped.

Referring to Fig. 2, tip chaser "B" slightly, and lap cutting edge of both chasers, as in Fig. 3, taking care not to twist chaser "B". Take only about eight strokes, then test for results. Further lapping may be

necessary, however too much can ruin thread form or cause other troubles.

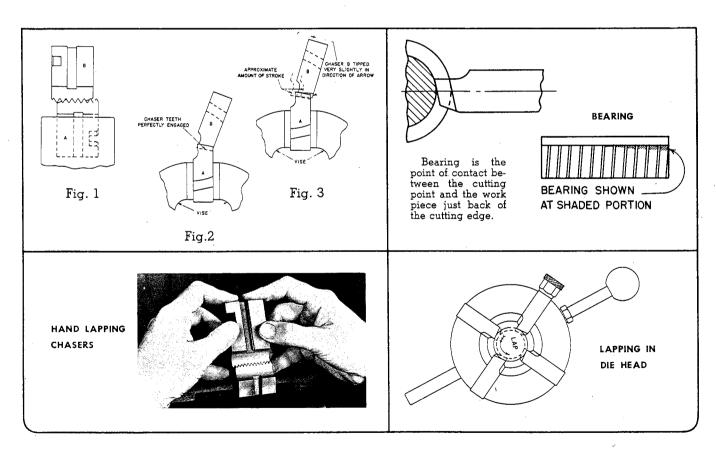
Tapped chasers are almost always lapped in a die head. Milled chasers may also be lapped in a die head but usually by hand.

Chasers are lapped in a die head by running lap in reverse direction. It is recommended that the lap used be a good sample. If necessary to make a lap be sure to obtain a good thread.

Fine emery and oil are also used for a lapping compound, tension is applied by closing the die head slightly on the lap.

Very few turns of the lap are required and be careful not to lap too much.

Clean chasers and die head thoroughly after lapping and before using to cut a thread.



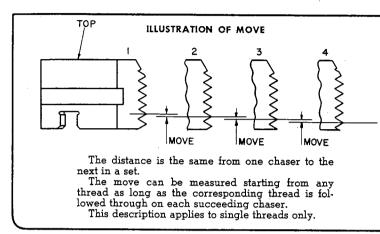
CHASERS TOO KEEN

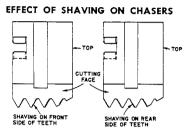
One of the causes for stripped threads not covered elsewhere is that the chasers may be too keen. In this case dull the chaser teeth at the chamfer. This is usually done by stoning lightly. It is most often necessary to do this when threading brass and zinc.

SHAVING

A set of chasers consists of four or more cutters which together produce the full thread (helical groove) on the work place. To accomplish this, the chasers have to have ''move'' or advance of the teeth from one chaser to the next. ''Shaving'' means that

not all the chasers are "tracking" properly or following exactly in the groove cut by the preceding chaser or chasers. While the thread form on each chaser might be good, the thread they cut, combined, could be too thin or of incorrect form.





The chaser or chasers that are shaving can be detected by noting the frosting on the cutting face along the front or back edges of the teeth. This frosting appears as a narrow band and indicates that these cutting edges have been taking a light shaving cut.

Chasers may be corrected for shaving by lapping as described on the opposite page. Only the chasers that are shaving are to be lapped. In some cases only one chaser has to be corrected and when rubbing, care should be taken not to pass it across the cutting face of the mating chaser or this chaser may be forced out of trackage.

With milled chasers take the chaser that is shaving, hold it in the fingers and force sidewise or twist slightly in such a manner as to lap the sides of the teeth that show frosting. To correct shaving, the lapping will not be carried across the full width of the land, but only along the cutting edge of chaser.

After lapping remove the frosting from the cutting

face by stoning lightly with an oil store and cut a sample or two. If the frosting again appears, the chasers must be lapped an additional amount.

Tapped form chasers are usually lapped in a die head as described on opposite page. They may also be lapped on a sample held in a vise.

Frequently, machine operators stone chasers for shaving. We recommend lapping; but stoning, if expertly done, will correct the condition and may be accomplished much more quickly. Only the sides of teeth showing frosting should be stoned. Stoning should be done lightly and at the sides of teeth along the cutting edge. Use a diamond shaped or knife-edge stone.

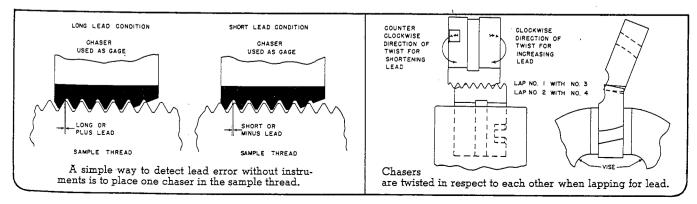
LEAD ERROR

Lead error is usually detected when a finished piece will not pass the gage and a check with a thread comparator or lead indicator shows lead error.

The correction of lead errors depends upon the cause. The procedures are either self evident or have been discussed elsewhere.

However, should it be necessary to correct chasers for lead, it is possible to lap them so that they will produce threads within closer lead limits.

In lapping chasers for lead, follow the same general instructions as rubbing chasers for bearing.



Servicing

BREAKAGE

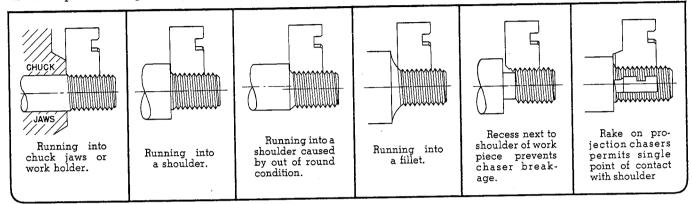
The most frequent threading accident is chaser breakage. Usually we find that the chasers have run into something — we call it 'Running into a shoulder.''

It may not actually be a shoulder, it may be any of the conditions shown on this page.

The remedy for actually running into a shoulder is to stop far enough away from the shoulder or

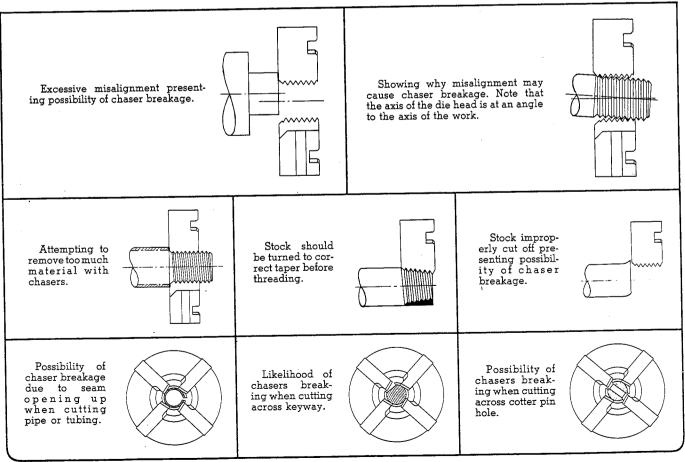
chuck, or to recess the work piece in front of the shoulder.

Projection chasers can frequently be used to advantage on shoulder threading. A 5° rake ground on top of the projection is recommended. This rake permits the chasers to cut into the shoulder and are less apt to break in event of accidentally striking against one.



Misalignment, heavy bearing, improper face grinds, improper chamfers, attempting to thread stock not turned to size prior to threading, improper adjust-

ment of chasers to size and conditions peculiar to the work piece may also cause chaser breakage. Some of these conditions are illustrated below.



TAPS

Collapsing

| Chasers | • | | • | • | • | 48-49 |
|---------|---|--|---|---|---|-------|
| | | | | | | |
| | | | | | | |

Disassembly 45–46

Replacement Parts . . . 46

Setting Up 44-45

Solid Adjustable 47

taps



COLLAPSING

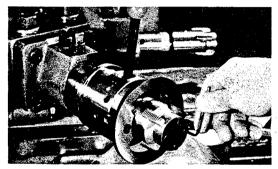
The principle of a Geometric collapsing tap is to collapse the chasers at the end of the cut, releasing the chasers from the work, thus permitting the return of the tap without reversing the spindle or following the lead of the thread. The proper care and operating

conditions for these tools are so similar to those described for self opening Die Heads, that we recommend a thorough reading of the section on ''General Instructions'' pages 6-7.

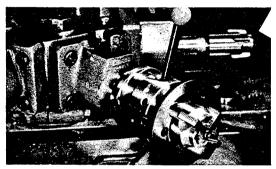
Setting up for Operation

1. INSERTING CHASERS

Before you can insert the chasers the cap must be removed from the nose of the tool by removing cap screws and the tap should be set into cutting position. Then insert the chasers in the proper slots: The No. 1 chaser in the slot stamped No. 1, the No. 2 chaser in the slot stamped No. 2, and so on. Be sure chasers are fitted on ribs on plunger.



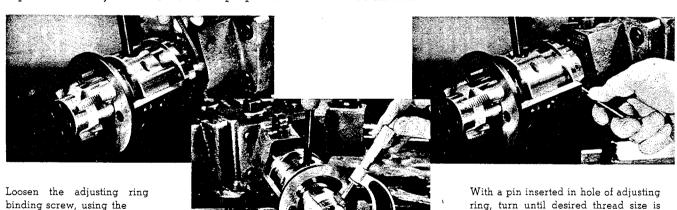
(Shown with chasers in position) Remove cap screws with the hex key. Lift off cap.



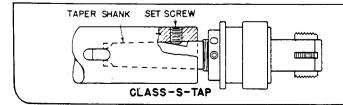
Be sure tap is in cutting position by pulling forward on closing handle until tap locks.

2. ADJUSTING CHASERS TO SIZE

The cap should of course be put back on the nose of the tool and cap screws inserted. Then you are in a position to adjust the chasers to proper size. Micrometers can be used to set the chasers to size, the adjustment to proper diameter being accomplished as shown.



Using Micrometer to Obtain Desired Thread Size



When using a tool with a Morse Taper shank don't attempt to drive with the tang alone. Drill and tap a hole in the machine spindle, using a set screw to locate the tool securely in the spindle.

ing screw.

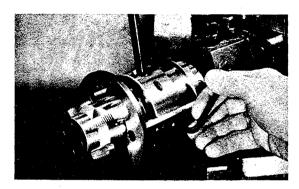
obtained. Tighten adjusting ring bind-

hex key provided.

3. SETTING OPERATING STOP

The tap must also be set so as to cut the proper length of thread. On a turret lathe and with some rotating tools this usually means the setting of the trip plate so as to contact the work or the work-holding fixture at the proper moment. On some automatic machines a yoke or fork is employed.

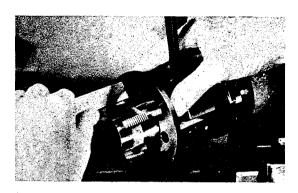
In setting up a collapsing tap allow at least 3/6" for the collapsing action of the tool. In other words,



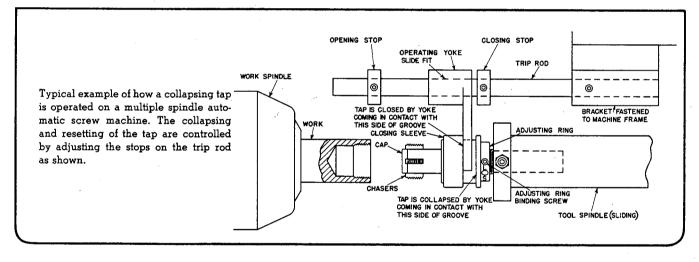
Loosen the trip bar binding screws with the hex key provided.

set the trip plate (if used) so that the distance from the front of chasers to trip plate measures at least 3/6" less than the depth desired. In case of a yoke trip allow a like amount. This is extremely important if tapping to a shoulder or blind bottom. Minor adjustments can be made after the first thread is cut.

It is good practice before cutting a thread to reset and trip the tap once or twice by hand to be sure the tool is functioning properly.



Move the plate to stop position. Tighten the trip bar binding screw securely.



- 5. PROPER SPEED This subject is covered fully in Self-Opening Die section. See pages 8-9.
- **6. PROPER LUBRICANT** This subject is covered fully in Self-Opening Die section. See page 10.

Disassembly

Take off the cap by removing cap screws. Remove the trip plate complete with trip bars by removing the two trip bar screws. Remove the closing handle by driving out the handle pin.

This pin can most easily be driven out from the left when facing front of tap. Next, back out the plunger screw which will release the plunger spring and washer. If the tap has a Morse Taper shank, the tang must first be removed. The tang is threaded into the end of the shank and cross pinned. Then loosen the adjusting ring binding screw and unscrew the adjusting ring and slide it over the tap shank. If the tap is arranged with a shank bushing or flanged shank, it must be taken off to permit removal of parts.

Next remove the closing sleeve trip screw and slide the closing sleeve off the skeleton ring and take it off over the tap shank. When sliding the closing sleeve off the skeleton ring be sure to hold the pawl under tension until the closing sleeve is removed, after which the pawl and pawl springs can be released. Note that the

(continued on next page)



COLLAPSING

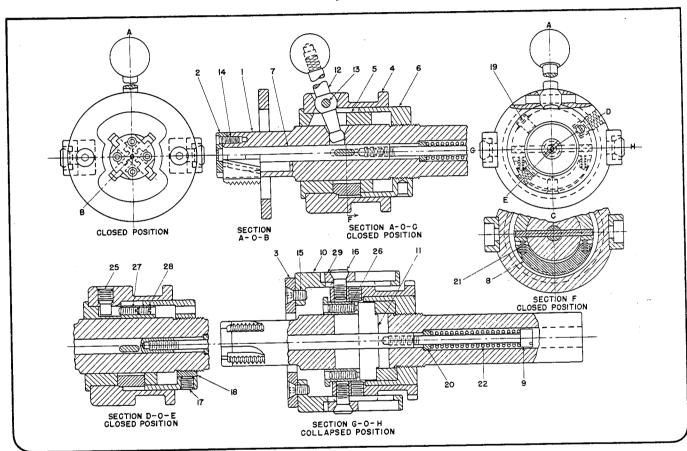
(Continued from preceding page)

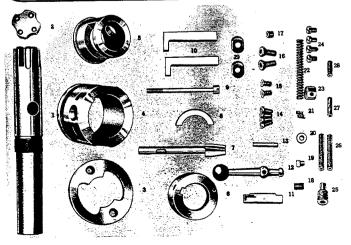
pawl has the beveled edge toward the front of the tap. Now back off the two plunger key screws about 1/4" from the front face of the skeleton ring. Do not disturb the abutment screw and abutment lock screw located in the back face of the skeleton ring, inasmuch as these control the positive action of the tap and have been properly set at the factory. The plunger key can now be taken out by pushing it across the tap and this will disengage the skeleton ring which can now be taken off over the tap shank. The plunger can be removed by pushing it out through the front of the tap.

To assemble the tap, reverse the sequence of operations.

REPLACEMENT PARTS

Style S





PARTS FOR COLLAPSIBLE TAP — STYLE S

When ordering repair parts give both number and name of part, also construction number and serial number of the tool.

- Skeleton (Specify shank size
- when ordering).
 Cap.
 Trip plate.
 Closing sleeve.
 Skeleton ring.
 Adjusting ring.
 Plunger. 4 5 †6 7
- Plunger.
 Pawl.
 Plunger screw.
 Trip bars.
 Plunger key.
 Closing handle.
 Closing handle pin.
 Cap screws.
- Trip plate screws.

- Trip bar screws.

 Adjusting ring binding 16 17
- SCIEW. Adjusting ring binding

- Adjusting ring billioning shoe.

 Skeleton ring key.
 Plunger screw washer.
 Pawl springs.
 Plunger spring.
 Closing sleeve plug.
 Closing sleeve screws.
 Closing sleeve trip screw.
 Plunger key screws.
 Abutment screw.
- Abutment screw.
 Abutment lock screw.
 -Trip Bar Binding Shoes
- *Cap as shown is a regular cap for use with regular chasers. If tapping to a blind bottom or broad shoulder specify a bottoming cap for use with overhanging chasers.

†Furnished assembled with No. 17 and No. 18.

SOLID ADJUSTABLE

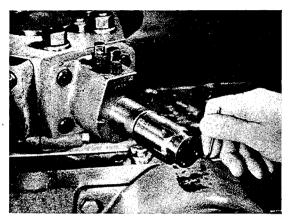




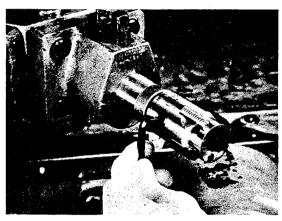
GENERAL INSTRUCTIONS

Solid Adjustable taps differ from Collapsible Taps in that, while adjustable, the chasers do not collapse in the tap. Like Solid one piece taps they must be backed off the work when in use.

The same type of chasers are employed in these



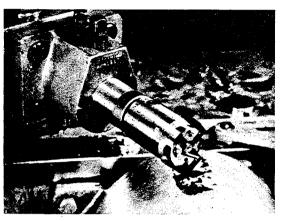
To insert or remove chasers, first remove cap screws and cap.



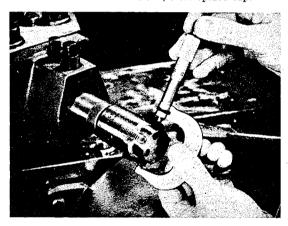
To adjust for size, loosen one adjusting screw and tighten the opposing screw. Be sure both screws are tight before starting to tap.

taps as in Collapsible taps, in fact they are interchangeable size for size.

For threading bottoming holes a 'bottoming' cap should be employed which permits the chasers to project or 'overhang' slightly beyond the nose of the tap.

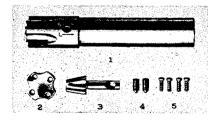


2. Insert chaser number 1 in slot number 1, chaser number 2 in slot 2, etc. Replace cap.

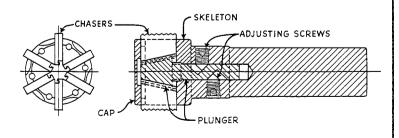


 Chasers may be measured for size with a micrometer during and after adjustment.

REPLACEMENT PARTS — STYLE SJ



- 1. Skeleton (Specify shank size when ordering)
- 2. Cap (If used with overhanging chasers, specify overhanging cap)



- 3. Plunger
- 4. Adjusting Screws
- 5. Cap Screws

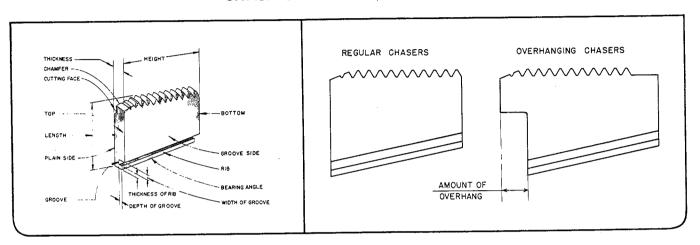


Geometric Class S Tap Chasers are interchangeable size for size in all types of Geometric Taps. They may be 'regular" or 'overhanging" chasers. For tapping to a blind bottom or to a shoulder, overhanging chasers and a bottoming cap are required.

While there are many differences in the problems involved in external and internal threading, many of the factors which govern the successful use of Die Head Chasers are also true of Tap Chasers. We therefore recommend reading the section on Die Head Chasers for the basic principles of their function, operation and care.

The information on this and the opposite page however refer specifically to tap chasers.

CHASERS FOR S AND SJ TAPS



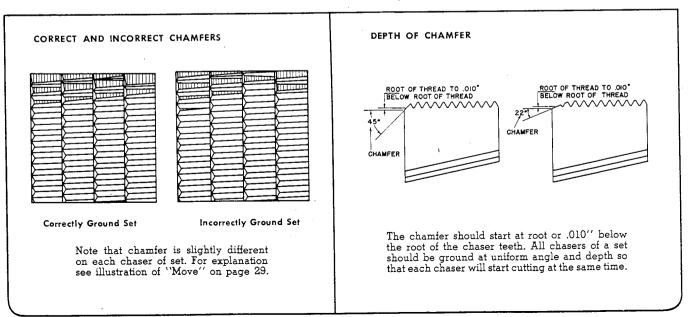
SHARPENING CHASERS

Nothing contributes more to the production of accurate threads, and low cost per thread, than accurate sharpening of chasers. Frequent light grinding or touching up will not only give better threads but will greatly extend the life of the chasers. Partial dullness leads to chipping as well as poor threads.

Therefore, to obtain the best results from any chasers they should be sharpened periodically and before they become dull. They should be resharpened by machine using an appropriate grinding fixture. They should not be resharpened free hand.

See pages 35 thru 39 for sharpening fixture.

Chamfer Grinding



Grinding Cutting Face

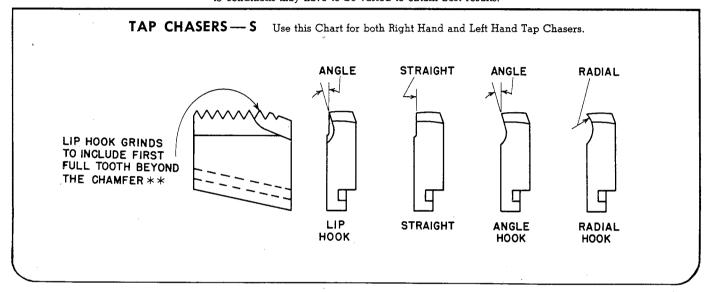
Never grind chasers free hand. Always use a grinding fixture or grind them on a surface grinder equipped with a suitable work holder. The usual procedure is to employ a magnetic chuck on a surface grinder which permits resharpening all chasers of a set at one set-up. This, of course, insures equal resharpening of all chasers.

It is important that the width of the land or thickness of cutting edge should be uniform on all chasers of a set or the load of cutting will be thrown entirely upon the thicker chaser or chasers.

Before setting up, be sure you know what face grind should be employed. Use the chart below as a guide.

TAP CHASER GRINDING CHART FOR FACE GRINDING ONLY

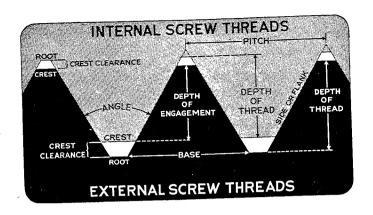
The Cutting Face Grinds specified are approximate and due to conditions may have to be varied to obtain best results.

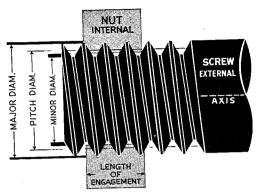


**Lip Hook Grinds not recommended for Shoulder or Bottoming Work, in this case use the same angle but omit the lip.

| Material | Straight Thread | Taper Thread | Material | Straight Thread | Taper Thread |
|------------------------|------------------|-----------------|-----------------------------------|-----------------|-----------------|
| Aluminum – Cast | 20° Radial Hook | 20° Radial Hook | Magnesium | 20° Radial Hook | 20° Radial Hook |
| Aluminum – Die Cast | 20° Radial Hook | 20° Radial Hook | Monel Metal | 10° Hook | 10° Hook |
| Aluminum – Rod | 20° Radial Hook | 20° Radial Hook | Nickel | 20° Lip Hook | 15° Radial Hook |
| Aluminum — Stamping | 20° Radial Hook | 20° Radial Hook | Rubber | 5° Hook | 5° Hook |
| Bakelite | 5° Hook | 5° Hook | Silver – German | 10° Hook | 10° Hook |
| Brass – Bar | 5° Hook | 5° Hook | Steel – Bessmr. Scr. Stock | 10° Hook | 10° Hook |
| Brass – Cast | 5° Hook | 5° Hook | Steel – Cast | 10° Hook | 10° Hook |
| Brass — Forging | 10° Hook | 10° Hook | Steel – Carb. SAE 1010–1035 | 10° Hook | 10° Hook |
| Brass – Stamping | 10° Hook | 10° Hook | Steel – Carb. SAE 1112–X1340 | 10° Hook | 10° Hook |
| Brass — Tubing | 10° Hook | 10° Hook | Steel – Carb. SAE 1040–1095 | 20° Lip Hook | 15° Radial Hook |
| Brass — Naval | 10° Hoo k | 10° Hook | Steel - Mang. SAE T1330-T1350 | 20° Lip Hook | 15° Radial Hook |
| Bronze – Bar | 10° Hook | 10° Hook | Steel - Chrome SAE 5120-52100 | 20° Lip Hook | 15° Radial Hook |
| Bronze – Cast | 5° Hook | 5° Hook | Steel – Chrome Van. SAE 6115-6195 | 20° Lip Hook | 15° Radial Hook |
| Bronze – Cast Aluminum | 10° Hook | 10° Hook | Steel - Forging | 20° Lip Hook | 15° Radial Hook |
| Bronze – Manganese | 10° Hook | 10° Hook | Steel - Molybdenum SAE 4130-4820 | 20° Lip Hook | 15° Radial Hook |
| Bronze - Naval | 10° Hook | 10° Hook | Steel - Nickel SAE 2015-2515 | 20° Lip Hook | 15° Radial Hook |
| Bronze – Phosphor | 10° Hook | 10° Hook | Steel - Ni-Chrome SAE 3115-3450 | 20° Lip Hook | 15° Radial Hook |
| Bronze – Tubing | 10° Hook | 10° Hook | Steel - Nitralloy | 20° Lip Hook | 15° Radial Hook |
| Celluloid | 5° Hook | 5° Hook | Steel – Stainless | 20° Lip Hook | 15° Radial Hook |
| Copper | 20° Lip Hook | 20° Radial Hook | Steel – Stamping | 20° Lip Hook | 15° Radial Hook |
| Everdur | 10° Hook | 10° Hook | Steel – Tool | 20° Lip Hook | 15° Radial Hook |
| Fibre | 5° Hook | 5° Hook | Steel – Tubing | 20° Lip Hook | 5° Hook |
| Iron – Cast | 5° Hook | 5° Hook | Steel – Semi-Casting | 5° Hook | 5° Hook |
| Iron — Malleable | 10° Hook | 10° Hook | Zinc – Die Casting | 20° Radial Hook | 20° Radial Hook |
| Iron – Wrought | 10° Hook | 10° Hook | • | | |

SCREW THREAD TERMS





Allowance. An intentional difference in the dimensions of mating parts. It is the minimum clearance or the maximum interference which is intended between mating parts.

Angle of Thread. The angle included between sides of thread, measured in an axial plane.

Axis of Screw. The longitudinal central line through the screw from which all corresponding parts are equally distant.

Base of Thread. The bottom section of a thread; the greatest section between the two adjacent roots.

Basic. The theoretical or nominal standard size from which all variations are made.

Crest. The top surface joining the two sides or flanks of a thread.

Crest Clearance. The space between the crest of a thread and the root of its component.

Depth of Thread. In profile, distance between crest and base measured normal to the axis.

Engagement, Depth of. The radial distance between crests of mating parts.

Engagement, Length of. The length of contact between two mating parts measured axially.

Helix Angle. The angle made by the helix of the thread at the pitch diameter with a plane perpendicular to the axis.

Lead. The distance a screw thread advances axially in one turn. (See Thread.)

Lead Error. The variation from basic lead.

Limits. The extreme dimensions which are prescribed to provide variation in fit and workmanship.

Major Diameter. On a straight screw thread the major diameter is the largest diameter of the screw or nut.

Minor Diameter. On a straight screw thread the smallest diameter of the screw or nut.

Neutral Zone. A positive allowance clearance. (See "Allowance.")

Number of Threads. The number of threads in one inch of length. Equals 1/pitch.

Pitch. The distance from a point on a screw thread to a corresponding point on the next thread measured parallel to the axis.

Pitch Diameter. On a straight screw thread the diameter of a cylinder where the width of the thread and the width of the space between threads is equal.

Root. The bottom surface joining the sides of two adjacent threads.

Screw Thread. A ridge of uniform section in the form of a helix on the external or internal surface of a cylinder, or as a conical spiral on the external or internal surface of a cone.

Side or Flank of Thread. The surface of the thread which connects the crest with root.

Taper Thread. A thread on which the pitch diameter is increased by some constant ratio as on the American Standard Taper Pipe Tap.

Thread, Single. A thread in which lead is equal to pitch.

Double. A thread in which lead is equal to twice the pitch.

Triple. A thread in which lead is equal to three times the pitch.

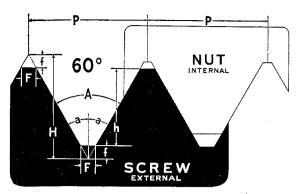
Quadruple. A thread in which lead is equal to four times the pitch.

Straight Thread. A thread on which the pitch diameter is the same from one end to the other.

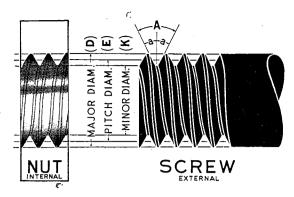
Thread, V. A theoretical form of thread having 60° angle and sharp top and bottom. Useful only as a basis for laying out other thread forms.

Tolerance. The amount of variation permitted in the size of a part. A tolerance may be expressed as plus or minus, or both.

THREAD DIMENSIONS . AMERICAN NATIONAL FORM



Adopted by the National Screw Thread Commission and formerly known as "United States Standard" this form of thread is the most common in the United States and one of the most widely used thread forms in the world. There are two standard series in commercial use — NC (National Coarse) and NF (National Fine). Threads of this form not included in the NC and NF series are designated as NS (National Special).



A = 60° = Angle of thread a = 30° = ½ Angle of thread F = 0.125000p, or ½p = Width of flat at crest and root f = 0.108253p, or ½H, or 1 6h = Depth of truncation H = 0.866025p = Depth Theoretical V 60° thread

h = 0.649519p, or 6.8H = Depth American National form thread

n = Number threads per inch

p = 1 in, = Pitch

| n | h | F | р | n | h | F | р |
|-------|-------|-------|---------|------|-------|-------|-------|
| 4 | .1624 | .0313 | .2500 | 18 | .0361 | .0069 | .0556 |
| 4 1/2 | .1443 | .0278 | .2222 | . 20 | .0325 | .0063 | .0500 |
| 5 | .1299 | .0250 | .2000 | 24 | .0271 | .0052 | .0417 |
| 6 | .1083 | .0208 | .1667 | 28 | .0232 | .0045 | .0357 |
| 7 | .0928 | .0179 | .1429 | 32 | .0203 | .0039 | .0313 |
| 8 | .0812 | .0156 | .1250 | 36 | .0180 | .0035 | .0278 |
| 9 | .0722 | .0139 | .1111 | 40 | .0162 | .0031 | .0250 |
| 10 | .0650 | .0125 | .1000 ' | 44 | .0148 | .0028 | .0227 |
| 11 | .0590 | .0114 | .0909 | 48 | .0135 | .0026 | .0208 |
| 12 | .0541 | .0104 | .0833 | 56 | .0116 | .0022 | .0179 |
| 13 | .0500 | .0096 | .0769 | 64 | .0101 | .0020 | .0156 |
| 14 | .0464 | .0089 | .0714 | 72 | .0090 | .0017 | .0139 |
| 16 | .0406 | .0078 | .0625 | 80 | .0081 | .0016 | .0125 |

UNIFIED THREADS Inasmuch as the Unified Thread is essentially the same as the American National Thread (differing only in product limits), Geometric tools are capable of producing either standard as there are adjustment facilities in all Geometric Tools whereby the pitch diameter of all threads produced can be controlled . . . Our handbook "SCREW THREADS" which covers classes of threads in both Unified and American National standards, is available on request.

HELIX ANGLES (BASED ON PITCH DIAMETER)

| | | <u> </u> | | | | | | | |
|--------------------------|--------|----------------------------------|--------|----------------------------------|--------|--------------------|--------|--------------------|---|
| Thread Size | Helix | Thread Size | Helix | Thread Size | Helix | Thread Size | Helix | Thread Size | Helix |
| # 0 — 80 | 4° 23′ | # 8 — 32 | 3° 58′ | 7/16 — 20 | 2° 15′ | 11/8 7 | 2°31′ | $2\frac{1}{2}$ — 4 | 1°57′ |
| # 1 — 64 | 4°31′ | # 8 — 36 | 3° 28′ | 1/2 — 13 | 3° 7′ | 1 1/8 — 12 | 1°25′ | 21/2 — 8 | 0° 57′ |
| # 1 — 72 | 3° 57′ | #10 24 | 4° 39′ | 1/2 20 | 1° 57′ | 11/4 7 | 2° 15′ | $2\frac{3}{4} - 4$ | 1° 46′ |
| # 2 56 | 4° 22′ | #10 32 | 3° 21′ | %6 12 | 2° 59′ | 11/4 12 | 1° 16′ | 2¾ — 8 | 0° 51′ |
| # 2 64 | 3° 45′ | #12 24 | 4° 1′ | %16 — 18 | 1° 55′ | 13/8 — 6 | 2° 24′ | 3 — 4 | 1°36′ |
| <u>#</u> 3 — 48 | 4° 26′ | #12 — 28 | 3° 22′ | 5⁄8 — 11 | 2° 56′ | 1 3/8 — 12 | 1° 9′ | 3 — 8 | 0° 47′ |
| # 3 — 56 | 3° 43′ | 1/4 — 20 | 4° 11′ | 5⁄8 — 18 | 1°43′ | 1½ — 6 | 2°11′ | 31/4 4 | 1°29′ |
| _# 4 — 4 0 | 4° 45′ | ¹ ⁄ ₄ — 28 | 2° 52′ | ³ / ₄ — 10 | 2° 40′ | 1 ½ — 12 | 1° 3′ | 31/2 — 4 | 1°22′ |
| # 4 48 | 3°51′ | 5⁄16 — 18 | 3° 40′ | $\frac{34-16}{}$ | 1°36′ | $1\frac{3}{4}$ — 5 | 2° 15′ | 3¾ — 4 | 1° 16′ |
| # 5 — 40 | 4°11′ | 5/16 — 24 | 2° 40′ | 7 ⁄8 — 9 | 2°31′ | 13/4 — 10 | 1° 5′ | 4 — 4 | 1°11′ |
| # 5 — 44 | 3° 45′ | ³⁄8 — 16 | 3° 24′ | 7 ⁄8 −− 14 | 1°34′ | $2 - 4\frac{1}{2}$ | 2° 11′ | | *************************************** |
| <u># 6 — 32</u> | 4° 50′ | ³ / ₈ — 24 | 2° 11′ | 1 — 8 | 2° 29′ | 21/4 — 41/2 | 1°55′ | | |
| # 6 40 | 3° 44′ | 7⁄16 — 14 | 3° 20′ | 1 —14 | 1°22′ | 21/4 - 8 | 1° 3′ | | |

AMERICAN NATIONAL AND UNIFIED STANDARD SIZES

| | | | | | Thread Series | | | |
|--------------------------------|-------------|--|-----------------|---------------|----------------|-------------|--------------|--|
| | Basic Major | NO C INO | NF & UNF | NEF | 8 N | 12 N & UN | 16 N & UN | 27 N |
| Diam. | Diam. | NC & UNC | | 14111 | | | | |
| 0 | .0600 | | 80 | | | | | |
| 1 | .0730 | 64 | 72 | | | | | |
| 2 | .0860 | 56 | 64 | | | | | |
| 3 | .0990 | 48 | 56 | | <u> </u> | | | |
| 4 | .1120 | 40 | 48 | | _ | | | |
| . 5 | .1250 | 40 | 44 | | | | | <u> </u> |
| 6 | .1380 | 32 | 40 | | | | | ļ |
| | .1640 | 32 | 36 | | | | | |
| 8 | .1900 | 24 | 32 | | | | | |
| 10 | | | 28 | | - | | | |
| 12 | .2160 | 24 | | 32 . | | | | 27 |
| 1/4 | .2500 | 20 | 28 | | | | | 27 |
| 5/16 | .3125 | 18 | 24 | 32 | | | | 27 |
| 3/8 | .3750 | 16 | 24 | 32 | | | | 27 |
| 7/16 | .4375 | 14 | 20 | 28 | | | | |
| 1/2 | ,5000 | 13 | 20 | 28 | | 12 | | 27 |
| | .5625 | 12 | 18 | 24 | | 12 | | 27 |
| 9/16 | .6250 | 11 | 18 | 24 | | 12 | | 27 |
| 5/8 | | | | 24 | | 12 | | |
| 11/16 | .6875 | 10 | 16 | 20 | _ | 12 | 16 | 27 |
| 3/4 | .7500 | 10 | 10 | 20 | | 12 | 16 | |
| 13/16 | .8125 | _ | | | | 12 | 16 | 27 |
| 7/8 | .8750 | 9 | 14 | 20 | | | 16 | |
| 15/16 | .9375 | | 1 | 20 | 1 | 12 | | 27 |
| 1 | 1.0000 | 8 | 12 | 20 | 8 | 12 | 16 | |
| 11/16 | 1.0625 | + | | 18 | | 12 | 16 | |
| | 1.1250 | 7 | 12 | 18 | 8 | 12 | 16 | |
| 11/8 | 1.1250 | | | 18 | | 12 | 16 | |
| 13/16 | | | 12 | 18 | 8 | 12 | 16 | |
| 11/4 | 1.2500 | 7 | 12 | 18 | | 12 | 16 | |
| 15/16 | 1.3125 | | | | | 12 | 16 | |
| 13/8 | 1.3750 | 6 | 12 | 18 | 8 | | 16 | |
| 17/16 | 1.4375 | 1 | | 18 | | 12 | | |
| 1½ | 1.5000 | 6 | 12 | 18 | 8 | 12 | 16 | |
| 19/16 | 1.5625 | | | 18 | | | 16 | |
| 15/8 | 1.6250 | | | 18 | 8 | 12 | 16 | |
| 17/8 | 1.6875 | | | 18 | | | 16 | |
| 111/16 | | | | 16 | 8 | 12 | 16 | |
| 13/4 | 1.7500 | 5 | | | | | 16 | |
| 113/16 | 1.8125 | | | | . 8 | 12 | 16 | |
| 17/8 | 1.8750 | | | | | 12 | 16 | |
| 2 | 2.0000 | 41/2 | | 16 | 8 | 16 | 16 | |
| 21/16 | 2.0625 | | | | | | | |
| 21/8 | 2.1250 | | | | 8 | 12 | 16 | |
| 2 ³ / ₁₆ | 2.1875 | | | | | | 16 | |
| | 2.2500 | 41/2 | | | 8 | 12 | 16 | |
| 21/4 | | */2 | | _ | | | 16 | |
| 25/16_ | 2,3125 | | - | - | | 12 | 16 | |
| 23/8 | 2.3750 | <u> </u> | | | | | 16 | |
| 27/16 | 2.4375 | | | | 8 | 12 | 16 | |
| 21/2 | 2.5000 | 4 | | | 8 | 12 | 16 | |
| 25⁄8 | 2.6250 | | | | | | 16 | |
| 23/4 | 2.7500 | 4 | | | 8 | 12 | | |
| 27/8 | 2.8750 | | | | | 12 | 16 | |
| 3 | 3.0000 | 4 | | | 8 | 12 | 16 | |
| 31/8 | 3.1250 | | | | | 12 | 16 | |
| | 3.2500 | 4 | | | 8 | 12 | 16 | |
| 31/4 | | | | | - | 12 | 16 | |
| 33/8 | 3.3750 | | | | 8 | 12 | 16 | |
| 31/2 | 3,5000 | 4 | | | | 12 | 16 | |
| 35/8 | 3.6250 | | | | | 12 | 16 | |
| 33/4 | 3.7500 | 4 | | | 8 | 16 | 16 | |
| 37/8 | 3.8750 | | | | | 12 | | |
| 4 | 4.0000 | 4 | | | 8 | 12 | 16 | |
| 41/4 | 4.2500 | | | | | 12 | 16 | |
| 41/ | 4.5000 | | | | · · | 12 | 16 | |
| 41/2 | | | | | | 12 | 16 | |
| 43/4 | 4.7500 | | | | | 12 | 16 | |
| 5 | 5.0000 | | | | | 12 | 16 | |
| 51/4 | 5.2500 | | | | | 12 | 16 | |
| 51/2 | 5.5000 | | | | | | 16 | |
| 53/4 | 5.7500 | | | | | 12 12 | 16 | -+ |
| | | | | 1 | 1 | 17 | 1 116 | 1 |

Bold type indicates Unified threads.

CLASSES 3A AND 3 EXTERNAL THREAD LIMITS

| | SIZE | | | CL | SS 3A UNIFI | ED | | | CLASS 3 A | MERICAN N | ATIONAL | |
|---------------------|-------------|--|----------|---------|-------------|--------|-------------------|----------|-----------|-----------|---------|-------------------|
| Nominal | Threads I | er Inch | Major Di | iameter | Pitch Di | ameter | Minor Diameter | Major Di | ameter | Pitch Di | ameter | Minor Diameter |
| | Coarse | Fine | Max. | Min. | Max. | Min. | Max. | Max. | Min. | Max. | Min. | Max. |
| 0 | | 80 | .0600 | .0568 | .0519 | .0506 | .0447 | .0600 | . 0566 | .0519 | . 0506 | .0447 |
| 1 | 64 | | .0730 | .0692 | .0629 | .0614 | .0538 | .0730 | .0692 | .0629 | .0615 | .0538 |
| 1 | | 72 | .0730 | .0695 | .0640 | .0626 | ,0560 | .0730 | .0694 | .0640 | .0627 | . 0560 |
| 2 | 56 | | .0860 | .0819 | .0744 | .0728 | .0641 | .0860 | . 0820 | . 0744 | . 0729 | .0641 |
| 2 | | 64 | .0860 | .0822 | .0759 | .0744 | .0668 | .0860 | .0822 | .0759 | . 0745 | .0668 |
| 3 | 48 | | .0990 | .0945 | . 0855 | .0838 | .0734 | . 0990 | . 0946 | . 0855 | . 0839 | . 0734 |
| 3 | | 56 | .0990 | .0949 | . 0874 | .0858 | .0771 | . 0990 | .0950 | .0874 | . 0859 | .0771 |
| 4 | 40 | | .1120 | .1069 | . 0958 | .0939 | .0813 | .1120 | .1072 | .0958 | .0941 | .0813 |
| .4 | | 48 | .1120 | .1075 | . 0985 | .0967 | .0864 | .1120 | .1076 | . 0985 | . 0969 | .0864 |
| 5 | 40 | | .1250 | .1199 | .1088 | .1068 | 0943 | .1250 | .1202 | .1088 | .1071 | .0943 |
| 5 | | 44 | .1250 | .1202 | .1102 | .1083 | .0971 | .1250 | .1204 | .1102 | .1086 | .0971 |
| 6 | 32 | | .1380 | .1320 | .1177 | .1156 | .0997 | .1380 | .1326 | .1177 | .1158 | . 0997 |
| 6 | | 40 | .1380 | .1329 | .1218 | .1198 | .1073 | .1380 | .1332 | .1218 | .1201 | .1073 |
| 8 | 32 | | .1640 | .1580 | 1437 | .1415 | .1257 | .1640 | .1586 | .1437 | .1418 | .1257 |
| 8 | T | 36 | .1640 | .1585 | .1460 | .1439 | .1299 | .1640 | . 1590 | .1460 | .1442 | .1299 |
| 10 | 24 | | .1900 | .1828 | . 1629 | .1604 | .1389 | .1900 | .1834 | . 1629 | , 1605 | .1389 |
| 10 | | 32 | .1900 | .1840 | .1697 | .1674 | . 1517 | .1900 | .1846 | . 1697 | . 1678 | .1517 |
| 12 | 24 | | .2160 | , 2088 | .1889 | .1863 | .1649 | .2160 | . 2094 | .1889 | . 1865 | .1649 |
| 12 | | 28 | .2160 | . 2095 | .1928 | .1904 | .1722 | .2160 | . 2098 | . 1928 | . 1906 | .1722 |
| 1/4 | 20 | | . 2500 | . 2419 | .2175 | 2147 | .1887 | . 2500 | . 2428 | . 2175 | .2149 | . 1887 |
| 1/4 | · | 28 | .2500 | . 2435 | . 2268 | . 2243 | . 2062 | . 2500 | . 2438 | . 2268 | . 2246 | . 2062 |
| 5/16 | 18 | · | .3125 | . 3038 | . 2764 | .2734 | . 2443 | .3125 | .3043 | . 2764 | . 2734 | . 2443 |
| 5/16 | · | 24 | .3125 | .3053 | . 2854 | . 2827 | .2614 | .3125 | .3059 | . 2854 | . 2830 | . 2614 |
| 3/8 | 16 | <u> </u> | .3750 | . 3656 | . 3344 | .3311 | . 2983 | .3750 | . 3660 | . 3344 | .3312 | . 2983 |
| 3/8 | · | 24 | .3750 | . 3678 | .3479 | .3450 | .3239 | . 3750 | . 3684 | . 3479 | . 3455 | .3239 |
| 7/16 | 14 | T | .4375 | .4272 | .3911 | .3876 | .3499 | . 4375 | . 4277 | .3911 | . 3875 | . 3499 |
| 7/16 | | 20 | .4375 | .4294 | . 4050 | .4019 | .3762 | .4375 | . 4303 | . 4050 | . 4024 | . 3762 |
| 1/2 | 13 | | .5000 | ,4891 | .4500 | .4463 | .4056 | .5000 | .4896 | .4500 | .4463 | .4056 |
| 1/2 | | 20 | .5000 | .4919 | . 4675 | .4643 | ,4387 | .5000 | . 4028 | . 4675 | . 4649 | . 4387 |
| 9/16 | 12 | | .5625 | .5511 | . 5084 | .5045 | .4603 | .5625 | .5513 | . 5084 | .5044 | . 4603 |
| 9/16 | | 18 | .5625 | . 5538 | .5264 | .5230 | . 4943 | . 5625 | . 5543 | . 5264 | . 5234 | . 4943 |
| 5/8 | 11 | 1 | .6250 | ,6129 | .5660 | .5619 | .5135 | . 6250 | .6132 | .5660 | .5618 | .5135 |
| 5/8 | 1 | 18 | .6250 | .6163 | .5889 | .5854 | . 5568 | .6250 | .6168 | . 5889 | . 5859 | .5568 |
| 3/4 | 10 | | ,7500 | .7371 | .6850 | . 6806 | ,6273 | .7500 | .7372 | . 6850 | .6805 | .6273 |
| 3/4 | | 16 | .7500 | .7406 | .7094 | .7056 | .6733 | .7500 | .7410 | .7094 | .7062 | .6733 |
| 7/8 | 9 | | .8750 | .8611 | .8028 | .7981 | .7387 | .8750 | .8610 | .8028 | .7979 | .7387 |
| 7/8 | <u> </u> | 14 | .8750 | .8647 | .8286 | .8245 | .7874 | .8750 | . 8652 | .8286 | .8250 | .7874 |
| 1 | 8 | | 1.0000 | .9850 | .9188 | .9137 | .8466 | 1.0000 | .9848 | .9188 | .9134 | .8466 |
| 1 | | 12 | 1.0000 | .9886 | .9459 | .9415 | .8978 | 1.0000 | .9888 | .9459 | .9419 | .8978 |
| 11/8 | 7 | | 1,1250 | 1.1086 | 1.0322 | 1.0268 | .9497 | 1.1250 | 1,1080 | 1.0322 | 1.0263 | .9497 |
| 11/8 | <u> </u> | 12 | 1.1250 | 1.1136 | 1.0709 | 1.0664 | 1.0228 | 1.1250 | 1.1138 | 1.0709 | 1.0669 | 1.0228 |
| 11/4 | 7 | | 1.2500 | 1.2336 | 1.1572 | 1.1517 | 1.0747 | 1.2500 | 1.2330 | 1.1572 | 1.1513 | 1.0747 |
| 11/4 | | 12 | 1.2500 | 1.2386 | 1.1959 | 1.1913 | 1.1478 | 1.2500 | 1.2388 | 1.1959 | 1.1919 | 1.1478 |
| 13/8 | 6 | | 1.3750 | 1,3568 | 1.2667 | 1.2607 | 1.1705 | 1.3750 | 1.3548 | 1.2667 | 1,2596 | 1.1705 |
| 13/8 | | 12 | 1.3750 | 1.3636 | 1.3209 | 1.3162 | 1.2728 | 1.3750 | 1.3638 | 1,3209 | 1.3169 | 1.2728 |
| 11/2 | 6 | | 1.5000 | 1.4818 | 1.3917 | 1.3856 | 1.2955 | 1.5000 | 1.4798 | 1.3917 | 1.3846 | 1.2955 |
| 11/2 | | 12 | 1.5000 | 1.4886 | 1.4459 | 1.4411 | 1.3978 | 1.5000 | 1.4888 | 1.4459 | 1.4419 | 1.3978 |
| 13/4 | 5 | 1 | 1.7500 | 1.7295 | 1.6201 | 1.6134 | 1.5046 | 1.7500 | 1.7268 | 1.6201 | 1.6119 | 1.5046 |
| 2 | 41/2 | | 2.0000 | 1.9780 | 1.8557 | 1.8486 | 1.7274 | 2.0000 | 1.9746 | 1.8557 | 1.8468 | 1.7274 |
| 21/4 | | | 2.2500 | 2.2280 | 2.1057 | 2.0984 | 1.9774 | 2.2500 | 2.2246 | 2.1057 | 2.0968 | 1.9774 |
| | 41/2 | | 2.5000 | 2.4762 | 2.3376 | 2.3298 | 2.1933 | 2.5000 | 2.4720 | 2.3376 | 2.3279 | 2.1933 |
| 21/2 | 4 | | + | 2.7262 | 2.5876 | 2.5797 | 2.4433 | 2.7500 | 2.7220 | 2.5876 | 2.5779 | 2.4433 |
| $\frac{2^{3}/4}{3}$ | 4 | | 2.7500 | | 2.8376 | 2.8296 | 2.6933 | 3.0000 | 2.9720 | 2.8376 | 2.8279 | 2.6933 |
| | 4 | | 3.0000 | 2.9762 | 3.0876 | 3.0794 | 2.9433 | 3.2500 | 3.2220 | 3.0876 | 3.0779 | 2.9433 |
| 31/4 | 4 | | 3.2500 | 3.2262 | 3.0876 | 3.0794 | 3.1933 | 3.5000 | 3.4720 | 3.3376 | 3.3279 | 3.1933 |
| 31/2 | 4 | ··- | 3.5000 | 3.4762 | - | 3.5792 | 3.1933 | 3.7500 | 3.7220 | 3.5876 | 3.5779 | 3.4433 |
| 33/4 | 4 | | 3.7500 | 3,7262 | 3.5876 | 3.8291 | 3.6933 | 4.0000 | 3.9720 | 3.8376 | 3.8279 | 3.6933 |
| 4 | 4 | | 4.0000 | 3.9762 | 3.8376 | 3.0491 | 3.0333 | 7.000 | 0.0120 | | 3.0220 | 1 0.000 |

PITCH DIAMETER TOLERANCES

PITCH DIAMETER TOLERANCES FOR EXTERNAL THREADS OF SPECIAL DIAMETERS, PITCHES AND LENGTHS OF ENGAGEMENT, CLASS 3A (UNS and NS Threads)

| | 6 5001 to 0000 | | | | | | :: | : : | | | .0041 | 0.0043 | 0.0045 | 0.0047 | 0.0049 | 0.0052 | 0,0055 | 0.0061 | 0.0068 | 0.0082 |
|-----------------------|---|----------------------------------|----------------------------------|---------------------------|------------|---------------------------|-------------------------------|-------------------------------|-------------------------------|---|---|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|--|--|
| | 5 4.5001 5. to 5.5000 7. | | | ::: | : : | | | | | | 0040 | | 0044 | 0045 | 0048 | 0020 | 0054 | 0059 | 0067 | 0.0081 |
| | 7501 4.9 to 5000 5.8 | :: | :: | :: | :: | :: | | | | 0.0036 | 0.0038 0. | 0.0041 | 00 | 0.0044 0. | 0.0046 0. | 0049 0.0054 | 0053 0. | 0058 0. | 0.0066 0. | 0.0079 0.0088 0 |
| - | € 4 | :: | | :: | | :: | :: | | : : | 0036 0.0 | - | | | | | 00 | 00 | .0057 .0063 0. | 0065 0. | 0.0079 0.0087 0. |
| - | _ი ო ო | : : | :: | | | | :: | :: | 3833 | 00 | 37 0.0037 40 0.0041 | 39 0.0040 43 0.0044 | 41 0.0041 44 0.0045 | 42 0.0043 46 0.0047 | 45 0.0045 49 0.0050 | 47 0.0048 52 0.0053 | 51 0.0052 56 0.0057 | 00 | 00 | |
| | 3 2.7501 to 3.2500 | | : : | | | | | | 0.0033 | 0.0035 | 6 0.0037 9 0.0040 | 9 0.0039 2 0.0043 | 0 0.0041 | 1 0.0042 5 0.0046 | 9 0.0045 0.0049 | 0.0047 | 0.0051 5 0.0056 | 0.0056 | 0 0.0064 | 7 0.0078 5 0.0086 |
| | 2.1/2 2.2501 to 2.7500 | | | | | | | : : | 0.0032 | 0.0034 | 0.0036 | 0.0038 | 0.0040 | 0.0041 | 0.0044 | 0.0046 | 0.0050 | 0.0055 | 0.0063 | 0.0077 |
| | 1.8751 to 2.2500 | | | | | | | : : | 0.0031 | 0.0033 | 0.0035 | 0.0037 | 0.0039 | 0.0040 | 0.0043 | 0.0045 | 0,0049 | 0.0054 | 0.0062 | 0.0076 |
| | 1 3/4 1.6251 to 1.8750 | : : | :: | : : | | | | : : | 0.0031 | 0.0032 | 0.0034 | 0.0036 | 0.0038 | 0.0040 | 0.0042 | 0.0045 | 0.0048 | 0.0054 | 0.0061 | |
| NCES | 11/2 1.3751 to 1.6250 | : : | | | | | : : | 0.0029 | 0.0030 | 0.0031 | 0.0033 0.0037 | 0.0036 | 0.0037 | 0.0039 | 0.0041 | 0.0044 | 0.0048 | 0.0053 | 0.0061 0.0067 | ::: |
| TOLERANCES | 1 1 /4 1, 1251 1, 1251 1, 3750 | : : | | : : | : : | : : | : : | 0.0028 | 0.0029 | 0.0031 | 0.0033 | 0.0035 | 0.0036 | 0.0038 | 0.0041 | 0.0043 | 0.0047 | 0.0052 | :: | : : . |
| DIAMETER | 0.8751 1 to 1.1250 1 | : : | | | | | 0.0026 | 0.0027 | 0.0028 | 0.0030 | 0.0032 | 0.0034 | 0.0036 | 0.0037 0.0041 | 0.0040 | 0.0042 | 0.0046 | 0.0051 | | ::: |
| PITCH DI | 3/4 0.6876 to 0.8750 | : : | : : | : : | 0.0022 | 0.0024 | 0.0025 | 0.0026 0.0029 | 0.0027 | 0.0029 | 0.0031 | 0.0033 | 0.0035 | 0.0036 | 0.0039 | 0.0041 | 0.0045 | : : | :: | |
| д | 5/8 0.5626 to 0.6875 | :: | : : | : : | 0.0022 | 0.0023 | 0.0025 0.0027 | 0.0026 | 0.0027 | 0.0028 | 0.0030 | 0.0032 | 0.0034 | 0.0036 | 0.0038 | 0.0041 | :: | : : | :: | |
| | 1/2 0.4376 to 0.5625 | : : | : : | 0.0020 | 0.0021 | 0.0022 | 0.0024 | 0.0025 | 0.0026 | 0.0028 | 0.0029 | 0.0032 | 0.0033 0.0037 | 0.0035 | 0.0037 | 0.0040 | :: | ::: | | |
| | 3/8 0.3126 to 0.4375 | : : | 0.0019 | 0.0019 | 0.0020 | 0.0022 | 0.0023 | 0.0024 | 0.0025 | 0.0027 | 0.0029 | 0.0031 | 0.0032 | 0.0034 | ::: | | ::: | ::: | :: | :: |
| | 0,2189 to 0,3125 | 0.0017 | 0.0018 | 0.0018 | 0.0019 | 0.0020 | 0.0022 | 0.0023 | 0.0024 | 0.0026 | 0.0028 | 0.0030 | : : | : : | :: | :: | :: | ::: | : : | ::: |
| | 3/16 0.1564 to 0.2188 | 0.0016 | 0.0017 | 0.0018 | 0.0019 | 0.0020 | 0.0021 | 0.0022 | 0.0024 | 0.0025 | 0.0027 | | :: | | : : | : : | 1 : : | ::: | :: | |
| | 1/8 0.1095 to 0.1563 | 0.0015 | 0.0016 | 0.0017 | 0.0018 | 0.0019 | 0.0021 | 0.0022 | 0.0023 | | ::: | : : | : : | | | ::: | ::: | | ::: | |
| | 3/32 0.0782 to 0.1094 | 0.0015 | 0.0016 | 0.0016 | 0.0017 | 0.0019 | : : | : : | ::: | :: | ::: | ::: | ::: | ::: | | : : | :: | ::: | ::: | |
| | | , | | | | | _ | | | | | 1 | 1 | T | T | | 1 | Τ., | T | :: |
| 1 | | 0.0014 | | | :: | : : | | | | | :: | ::: | | ::: | | | | | | |
| ement | 1/16 0.0600 to 0.0781 | to 0.19 0.0014 to 0.38 0.0016 | 0.21 0.0015 | 0.23 0.0016 | 0.27 | to 0.31 | 0.38 | 0.42 | to 0.47 | to 0.54 to 1.08 | to 0.62 to 1.24 | to 0.75 | to 0.83 to 1.66 | to 0.94 to 1.88 | to 1.07 to 2.14 | to 1.25 to 2.50 | to 1.50 to 3.00 | to 1.88 | to 2.50 | to 3.75 |
| of Engagement | 1/16 0.0600 to 0.0781 | | 0.0015 | 0.0016 | 27 | | 0.12 to 0.38 0.381 to 0.76 | 0.14 to 0.42 0.421 to 0.84 | 0.16 to 0.47 0.471 to 0.94 | 0.18 to 0.54 0.541 to 1.08 | 0.21 to 0.62 0.621 to 1.24 | 0.25 to 0.75 0.751 to 1.50 | 0.28 to 0.83 0.831 to 1.66 | 0.31 to 0.94 0.941 to 1.88 | 0.36 to 1.07 1.071 to 2.14 | 0.42 to 1.25 1.251 to 2.50 | 0.50 to 1.50 1.501 to 3.00 | 0.62 to 1.88 1.881 to 3.76 | 0.83 to 2.50 2.501 to 5.00 | 1.25 to 3.75 3.751 to 7.50 |
| Lengths of Engagement | 1/16 0.0600 to 0.0781 | to 0.19 to 0.38 | 07 to 0.21 0.0015 211 to 0.42 | to 0.23 0.0016 to 0.46 | 09 to 0.27 | 10 to 0.31 311 to 0.62 | 12 to 0.38 381 to 0.76 | 14 to 0.42 421 to 0.84 | 0.16 to 0.47 0.471 to 0.94 | lo 15 0.18 to 0.54 to 30 0.541 to 1.08 | to 15 0.21 to 0.62 to 30 0.621 to 1.24 | 25 to 0.75 751 to 1.50 | 28 to 0.83 831 to 1.66 | 31 to 0.94 941 to 1.88 | to 1.07 to 2.14 | to 1.25 to 2.50 | to 15 0.50 to 1.50 | 0.62 to 1.88 1.881 to 3.76 | 5 to 15 0.83 to 2.50 16 to 30 2.501 to 5.00 | 5 to 15 1.25 to 3.75 16 to 30 3.75 1 to 7.50 |

PITCH DIAMETER TOLERANCES FOR THREADS OF SPECIAL DIAMETERS, PITCHES AND LENGTHS OF ENGAGEMENT, CLASS 3

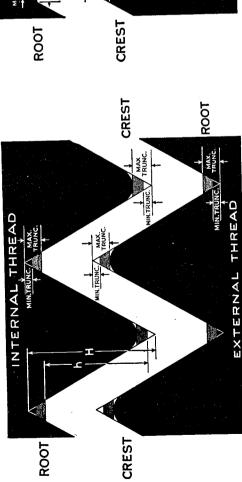
| | 6 5.5001 7.0000 | :: | :: | ::: | ::: | ::: | | ::: | ::: | : : | 0.0052 | 0.0054 | 0.0055 | 0.0057 | 0.0059 | 0.0061 | 0.0065 | 0.0070 | 0.0077 | 0.0090 |
|---------------|----------------------------------|-------------------------------|---------------------------|----------------------------|---------------------------|---------------------------------|---------------------------------|-----------------------------|-----------------------------|-----------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|------------------------------------|-------------------------------|-----------------------------|---------------------------|---------------------------------|
| | 5.5000 | :: | | | :: | ::: | :: | ::: | - : : | ::: | 0.0049 | 0.0051 | 0.0052 | 0.0054 | 0.0056 | 0.0058 | 0.0062 | 0.0067 | 0.0074 | 0.0087 |
| | 3.7501 to 4.5000 | :: | :: | : : | :: | ::: | ::: | | ::: | 0.0044 | 0.0046 | 0.0048 | 0.0049 | 0.0051 0.0057 | 0.0053 | 0.0055 | 0.0059 | 0.0063 0.0076 | 0.0071 | 0.0084 |
| | 31/2 3.2501 to 3.7500 | : : | : : | : : | ::: | | ::: | :: | ::: | 0.0042 | 0.0044 | 0.0046 | 0.0047 | 0.0049 | 0.0051 | 0.0053 | 0.0057 | 0.0061 | 0.0069 | 0.0082 |
| | 3 2.7501 to 3.2500 | :: | : : | :: | : : | ::: | :: | | 0.0039 | 0.0040 | 0.0042 | 0.0044 | 0.0045 | 0.0047 | 0.0049 | 0.0051 | 0.0055 | 0.0059 | 0.0067 0.0084 | 0.0080 |
| | 2.1/2 2.2501 to 2.7500 | :: | ::: | : : | : : | :: | :: | ::: | 0.0037 | 0.0038 | 0.0040 | 0.0042 | 0.0043 | 0.0045 | 0.0047 | 0.0049 | 0.0053 | 0.0057 | 0.0065 | 0.0078 |
| | 1.8751 to 2.2500 | :: | : : | :: | :: | :: | : : | ::: | 0.0035 | 0.0036 | 0.0038 | 0.0040 | 0.0041 | 0.0043 | 0.0044 | 0.0047 | 0.0050 | 0.0055 | 0.0062 | 0.0076 |
| | 13/4 1.6251 to 1.8750 | | :: | ::: | :: | :: | :: | :: | 0.0034 | 0.0035 | 0.0036 | 0.0038 | 0.0040 | 0.0041 | 0.0043 | 0.0046 | 0.0049 | 0.0054 | 0.0061 | |
| TOLERANCES | 1 1/2 1.3751 to 1.6250 | : : | : : | : : | :: | : : | :4: | 0.0031 | 0.0032 | 0.0033 | 0.0035 | 0.0037 | 0.0038 | 0.0040 | 0.0042 | 0.0044 | 0.0048 | 0.0052 | 0.0060 | :: |
| | 1 1 /4 1.1251 to 1.3750 | :: | : : | :: | :: | :: | :: | 0.0030 | 0.0031 | 0.0032 | 0.0033 | 0.0035 | 0.0037 | 0.0038 | 0.0040 | 0.0043 | 0.0046 | 0.0051 | | |
| DIAMETER | 0.8751 to 1.1250 | :: | | : : | ::: | :: | 0.0027 | 0.0028 | 0.0029 | 0.0030 | 0.0032 | 0.0034 | 0.0035 | 0.0037 0.0043 | 0.0039 | 0.0041 | 0.0045 | 0.0049 | : : | |
| PITCH I | 3/4 0.6876 to 0.8750 | :: | : : | :: | 0.0023 | 0.0024 | 0.0025 | 0.0026 | 0.0027 | 0.0028 | 0.0030 | 0.0032 0.0037 | 0.0033 | 0.0035 | 0.0037 | 0.0039 | 0.0043 | | : : | : : |
| | 5/8 0.5626 to 0.6875 | | : : | : : | 0.0022 | 0.0023 | 0.0024 | 0.0025 | 0.0026 | 0.0027 | 0.0029 | 0.0031 | 0.0032 | 0.0034 | 0.0036 | 0.0038 | : : | : : | : : | : : |
| | 1/2 0.4376 to 0.5625 | : : | : : | 0.0020 | 0.0021 | 0.0022 | 0.0023 0.0026 | 0.0024 | 0.0025 | 0.0026 | 0.0028 | 0.0030 | 0.0031 | 0.0033 | 0.0035 | 0.0037 0.0046 | : : | ::: | : : | : : |
| | 3/8 0.3126 to 0.4375 | :: | 0.0018 | 0.0019 | 0.0019 | 0.0020 | 0.0022 | 0.0023 | 0.0024 | 0.0025 | 0.0026 | 0.0028 | 0.0030 | 0.0031 | : : | : : | : : | : : | : : | ::: |
| | 1/4 0.2189 to 0.3125 | 0.0016 | 0.0016 | 0.0017 | 0.0018 | 0.0019 | 0.0020 | 0.0021 | 0.0022 | 0.0023 0.0027 | 0.0025 | 0.0027 0.0032 | : : | : : | : : | : : | | : : | : : | |
| | 3/16 0.1564 to 0.2188 | 0.0015 | 0.0015 | 0.0016 | 0.0017 | 0.0018 | 0.0019 | 0.0020 | 0.0021 | 0.0022 | 0.0024 | : : | : : | : : | :: | : : | : : | : : | | : : |
| | 1/8 0.1095 to 0.1563 | 0.0014 | 0.0014 | 0.0015 | 0.0016 | 0.0017 0.0019 | 0.0018 | 0.0019 | 0.0020 | : : | : : | : : | : : | | | | : : | : : | : : | : : |
| | 3.32 0.0782 to 0.1094 | 0.0013 | 0.0014 | 0.0014 | 0.0015 | 0.0016 0.0018 | : : | : : | | : : | ::: | : : 1 | | : : | : : | : : | : : | : : | | : : |
| | 1/16 0.0600 to 0.0781 | 0.0012 | 0.0013 | 0.0014 | 0.0014 | : : | : : | : : | :: | 7: : | : : | : : | : : | : : | : : | : : | : : | : : | | : : : : : : |
| of Engagement | Inches | 0.06 to 0.19 0.191 to 0.38 | 07 to 0.21 211 to 0.42 | .08 to 0.23 231 to 0.46 | 09 to 0.27 271 to 0.54 | 10 to 0.31 311 to 0.62 | .12 to 0.38 381 to 0.76 | . 14 to 0. 42 . 421 to 0.84 | .16 to 0.47 .471 to 0.94 | .18 to 0.54 .541 to 1.08 | 21 to 0.62 621 to 1.24 | 25 to 0.75 751 to 1.50 | 28 to 0.83 831 to 1.66 | 31 to 0.94 941 to 1.88 | 36 to 1.07 071 to 2.14 | 12 to 1.25 151 to 2.50 | 50 to 1.50 501 to 3.00 | 62 to 1.88 881 to 3.76 | 83 to 2.50 501 to 5.00 | 15 to 3.75 |
| Lengths of E | Number of Pitches | 5 to 15 0. | 5 to 15 0. | to 15 0. | to 15 0. | (5 to 15 0.1 (16 to 30 0.3 | (5 to 15 0.) (16 to 30 0.3 | to 15 0 | to 15 0 to 30 0 | to 15 0 to 30 0 | to 15 0. | to 15 0 | lo 15 0 | to 15 0 | lo 30 1. | { 5 to 15 0.42 { 16 to 30 1.251 | 5 to 15 0.50 6 to 30 1.501 | 5 to 15 0.6 16 to 30 1.8 | lo 15 0. | 5 to 15 1, 25 5 to 30 3, 751 |
| i I | Threads per Inch P | 80 | 72 (16 | 64 5 | 56 5 | 48 (16 | 40 { 16 | 36 (36 | 32 { 5 | 28 { 16 | 24 (5 | 20 (5 | 18 (5 | 16 (5 | 14 (5 | 12 { 5 | 10 (51 | 8 { 16 | 6 { 5 | 4 { 16 |

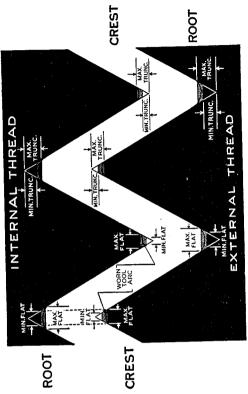
THREAD DIMENSIONS . PIPE

AMERICAN STANDARD AND DRYSEAL PIPE THREADS

American Standard Pipe Threads — NPT

American Standard Dryseal Pipe Threads — NPTF





Limits on Crest and Root of External and Internal Pipe Threads — Inches

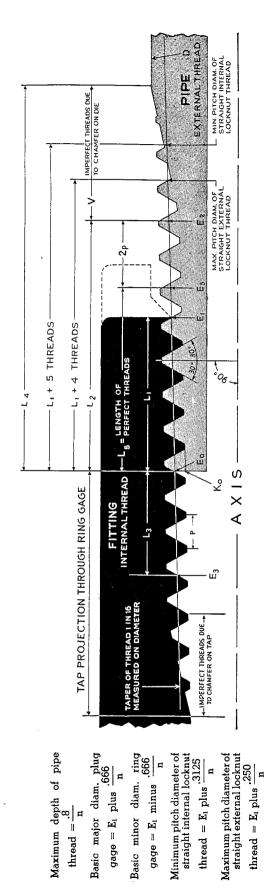
| | | 5 | T CRRCINETY | WARR TAPER PIPE THREAD | THREAD | | 1 | DRYSEAL PIPE THREAD | E THREAD | | |
|--------------|---------|-------------|-------------|------------------------|----------------|-----------------------------|---------|---------------------|---------------|------------|---------------------------------|
| | 1 | מ | ANDAR | | | | | | 2 | lonk | |
| THREADS | SHARP V | Depth Taper | Trunc | Truncation | Equiv Width | Equivalent Width of Flat | Trum | Truncation | Width of Flat | f Flat | |
| Per Inch | THREAD | ''Max' | Minimin | Maximum | Minimum | Maximum | Minimum | Maximum | Minimum | Maximum | |
| | | 7 | 5130 | 9000 | 0014 | 0041 | .0017 | .0035 | .0020 | .0040 | |
| 27 Crest | .03208 | .02903 | 2100. | 900 | .0014 | .0041 | .0035 | .0052 | .0040 | 990. | Note: The major diameter |
| Root | | | 200. | 9 | 200 | 0057 | 0036 | .0043 | 0030 | .0050 | of standard taper pipe plug |
| 18 Crest | .04811 | .04444 | 8100. | 0049 | 0021 | .005Z | .0043 | .0061 | .0050 | .0070 | gages and the minor diameter |
| Root | | | 9.00 | 9300 | 7,000 | 0064 | 0056 | .0043 | .0030 | .0050 | of standard taper pipe ring |
| 14 Crest | .06186 | .05714 | 9200 | 9500 | 0027 | .0064 | .0043 | .0061 | .0050 | .0070 | gages used for gaging dry- |
| Root | Culto | 75050 | £200. | 0063 | .0033 | .0073 | .0035 | .0052 | .0040 | 0900 | seal threads will be truncated. |
| 11 1/2 Crest | .07531 | 70600. | 0029 | .0063 | .0033 | .0073 | .0052 | .0078 | 0900 | 0600 0- | mum for all pitches. |
| Root | 50001 | 00001 | 0041 | .0078 | .0048 | 0600 | .0052 | 6900 | 0900 | 0800. | |
| 8 Crest | C7001. | 2001 | 0041 | .0078 | .0048 | 0600 | 6900' | .0095 | 0800. | .0110 | |
| Root | | | | | | | | | | | |

The limits specified above are intended to serve as a guide for establishing limits of the thread elements of taps, dies and thread chasers. These limits may be required on the product.

The Army-Navy Aeronautical Specifications AN-P-363 agrees with all values given in this table.

For complete specifications see latest edition of American Standards Association Pamphlet B.2-1.

THREAD DIMENSIONS . PIPE



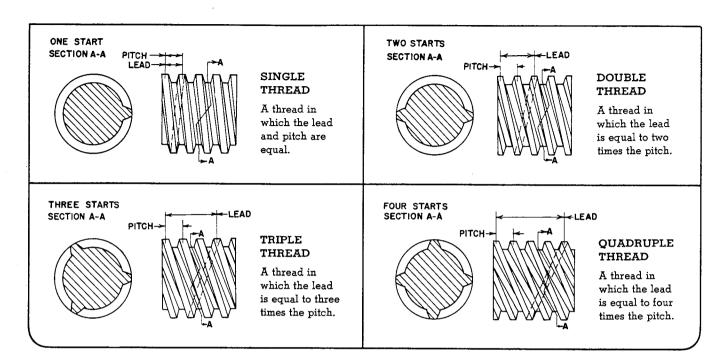
CANADARA,

Basic Dimensions of Taper Pipe Threads — Inches

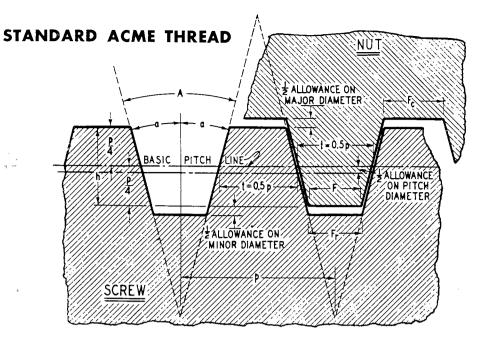
| | *TAP | DRILL | : | : R. 7. 8. 9. 7. 8. 9. 7. 8. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. |
|--------------------------------------|------------------------------|---|------------|---|
| | INCREASE IN DIAMETER | | : | .00231 .00231 .00347 .00347 .00446 .00543 1 .00543 1 .00543 1 .00543 1 .00781 .00781 .00781 .00781 .00781 .00781 .00781 .00781 |
| END | | Basic Minor Diameter | Κο | .2416 .3339 .4329 .5676 .7013 .9105 1.1441 1.7265 2.61995 2.61995 3.2406 3.7375 4.2344 5.2907 6.3461 8.3336 |
| SMALL END OF PIPE | | Pitch Diameter | Б | 27718 36351 47739 (61201 75843 96768 1.21363 1.79609 2.71953 3.34062 3.34062 3.34062 3.34359 4.33438 6.44609 8.43359 |
| THREADS | | Pitch Diameter of Largest External | ьű | .28287 .37537 .49556 .63056 .78286 .99286 .99286 .1.24543 1.83043 2.77500 3.40000 4.40000 6.52500 10.65000 |
| PERFECT THREADS | | Length | ű | .1870 .2907 .2907 .2907 .2909 .4029 .5029 .5329 |
| | TOTAL | LENGIH OF THREAD | Ľ | 3896 3924 5946 6006 7815 7935 10085 10085 110252 110252 110337 116337 116337 118337 119467 2.1467 2.1467 |
| | Internal | Pitch Diameter at Small End | E3 | .26424 .35656 .46697 .60160 .74504 .95429 1.19733 1.77978 2.25272 2.70391 3.32500 3.8218 4.31875 5.37511 6.43047 8.41797 |
| HREAD OF | Inte | Length Wrench Makeup | L3 | 11111 11111 11667 11667 2143 22143 22609 22609 22609 2250 2250 2250 2250 2250 2250 2250 22 |
| EFFECTIVE THREAD OR WRENCH MAKEUP | rnal | Pitch Diameter | মূ | .28750 .38000 .50250 .63750 .10179 .1.0179 .1.25630 .1.25630 .1.25630 .2.79062 .3.41562 .3.41562 .3.41562 .5.4062 .5.4062 .6.54062 .8.54062 .1.66562 |
| | External | Length, also Length of Plug Gage | Γ_2 | .2611 .2639 .4018 .4078 .5337 .5457 .6828 .7235 .7235 .7235 .7235 .7356 |
| right Ement | Basic Pitch Diam., also | ritch Diam. at Gaging Notch, also Basic Pitch Diam. of Straight Pipe Thread | Eı | .28118 .37476 .48989 .62701 .77843 .98887 1.23863 1.8234 2.29627 2.76216 3.38881 4.38712 5.4922 6.50597 8.50003 10.62094 |
| HAND TIGHT ENGAGEMENT | Length, also Thickness of | | L_1 | .160 .200 .200 .240 .320 .332 .420 .420 .420 .420 .682 .682 .682 .937 .937 .938 .1063 |
| H | | Length (| ъ | .03704 .03704 .03556 .05556 .05556 .07143 .07143 .08696 .08696 .08696 .12500 .12500 .12500 .12500 .12500 .12500 |
| PITCH | | Threads per Inch | u | 228884411111888888888888888888888888888 |
| PIPE SIZE | | Outside Diameter | D | .3125 .405 .540 .675 .840 1.050 1.315 1.315 1.315 2.375 2.375 3.500 4.500 4.500 6.625 8.625 8.625 1.0750 |
| PIPE | | Nominal | : | 111222848 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 |

* Methods of inspection vary. Care should be taken to use a tap drill or taper reamer which can meet thread specifications. Sizes given permit direct tapping without reaming the hole, but only give a full thread for the first two or three threads. See columns K₀ and L₂.

MULTIPLE THREADS



| | | | | Le | ead (given | in inches) | | | | |
|--------|--------|--------|--------|-----------|------------|-----------------|----------|-----------------|---------|------------|
| T.P.I. | Single | Double | Triple | Quadruple | Quintuple | Sextuple | Septuple | Octuple | Nonuple | Decuple |
| 3 | 1/3 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/3 | 2 2/3 | 3 | 3 1/3 |
| 4 | 1/4 | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 1 3/4 | 2 | 2 1/4 | 2 1/2 |
| 4 1/2 | 2/9 | 4/9 | 2/3 | 8/9 | 1 1/9 | 1 1/3 | 1 5/9 | 1 7/9 | 2 | 2 2/9 |
| 5 | 1/5 | 2/5 | 3/5 | 4/5 | 1 | 1 1/5 | 1 2/5 | 1 3/5 | 1 4/5 | 2 |
| 6 | 1/6 | 1/3 | 1/2 | 2/3 | 5/6 | 1 | 1 1/6 | 1 1/3 | 11/2 | $12/3^{-}$ |
| 7 | -1/7 | 2/7 | 3/7 | 4/7 | 5/7 | $\frac{-}{6/7}$ | 1 | $\frac{11/7}{}$ | 12/7 | 1 3/7 |
| 8 | 1/8 | 1/4 | 3/8 | 1/2 | 5/8 | 3/4 | 7/8 | 1 | 11/8 | 1 1/4 |
| 9 | 1/9 | 2/9 | 1/3 | 4/9 | 5/9 | 2/3 | 7/9 | 8/9 | 1 | 1 1/9 |
| 10 | 1/10 | 1/5 | 3/10 | 2/5 | 1/2 | 3/5 | 7/10 | 4/5 | 9/10 | 1 |
| 11 | 1/11 | 2/11 | 3/11 | 4/11 | 5/11 | 6/11 | 7/11 | 8/11 | 9/11 | 10/11 |
| 12 | 1/12 | 1/6 | 1/4 | 1/3 | 5/12 | 1/2 | 7/12 | 2/3 | 3/4 | 5/6 |
| 13 | 1/13 | 2/13 | 3/13 | 4/13 | 5/13 | 6/13 | 7/13 | 8/13 | 9/13 | 10/13 |
| 14 | 1/14 | 1/7 | 3/14 | 2/7 | 5/14 | 3/7 | 1/2 | 4/7 | 9/14 | 5/7 |
| 15 | 1/15 | 2/15 | 1/5 | 4/15 | 1/3 | 2/5 | 7/15 | 8/15 | 3/5 | 2/3 |
| 16 | 1/16 | 1/8 | 3/16 | 1/4 | 5/16 | 3/8 | 7/16 | 1/2 | 9/16 | 5/8 |
| 18 | 1/18 | 1/9 | 1/6 | 2/9 | 5/18 | 1/3 | 7/18 | 4/9 | 1/2 | 5/9 |
| 20 | 1/20 | 1/10 | 3/20 | 1/5 | 1/4 | 3/10 | 7/20 | 2/5 | 9/20 | 1/2 |
| 22 | 1/22 | 1/11 | 3/22 | 2/11 | 5/22 | 3/11 | 7/22 | 4/11 | 9/22 | 5/11 |
| 24 | 1/24 | 1/12 | 1/8 | 1/6 | 5/24 | 1/4 | 7/24 | 1/3 | 3/8 | 5/12 |
| 28 | 1/28 | 1 14 | 3/28 | 1/7 | 5/28 | 3/14 | 1/4 | 2/7 | 9/28 | 5/14 |
| 32 | 1/32 | 1/16 | 3/32 | 1/8 | 5/32 | 3/16 | 7/32 | 1/4 | 9/32 | 5/16 |
| 36 | 1/36 | 1/18 | 1/12 | 1/9 | 5/36 | 1/6 | 7/36 | 2/9 | 1/4 | 5/18 |
| 40 | 1/40 | 1/20 | 3/40 | 1/10 | 1/8 | 3/20 | 7/40 | 1/5 | 9/40 | 1/4 |
| 44 | 1/44 | 1/22 | 3/44 | 1/11 | 5/44 | 3/22 | 7/44 | 2/11 | 9/44 | 5/22 |
| 48 | 1/48 | 1/24 | 1/16 | 1/12 | 5/48 | 1/8 | 7/48 | 1/6 | 3/16 | 5/24 |
| 56 | 1/56 | 1/28_ | 3/56 | 1/14 | 5/56 | 3/28 | 1/8 | -1/7 | 9/56 | 5/28 |
| 60 | 1/60 | 1/30 | 1/20 | 1/15 | 1/12 | 1/10 | 7/60 | 2/15 | 3/20 | 1/6 . |



NOTATION

 $A = 29^{\circ}00'$

 $a = 14^{\circ}30'$

p = pitch

n = number of threads per inch

N = number of turns per inch

h = 0.5p, basic depth of thread

t = thickness of thread

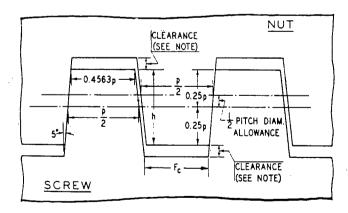
F = 0.3707p = basic width of flat

 $F_c = 0.3707p - 0.259 \times major diameter allowance$

 $F_r = 0.3707p - 0.259 \times \text{(minor diameter allowance on screw-pitch diameter allowance)}.$

| TPI(n) | h + allow. | F | Fr | р | TPI(n) | h + allow. | F | Fr | р |
|--------|------------|-------|-------|--------|--------|------------|-------|-------|-------|
| 1 | .5100 | .3707 | .3655 | 1.0000 | 51/2 | .1009 | .0674 | .0622 | .1818 |
| 11/3 | .3850 | .2780 | .2728 | .7500 | 6 | .0933 | .0618 | .0566 | .1667 |
| 1 1/2 | .3433 | .2471 | .2419 | .6667 | 7 | .0814 | .0530 | .0478 | .1429 |
| 2 | .2600 | .1854 | .1802 | .5000 | 8 | .0725 | .0463 | .0411 | .1250 |
| 21/2 | .2100 | .1483 | .1431 | .4000 | 9 | .0656 | .0412 | .0360 | .1111 |
| 3 | .1767 | .1236 | .1184 | .3333 | 10 | .0600 | .0371 | .0319 | .1000 |
| 31/2 | .1529 | .1059 | .1007 | .2857 | 12 | .0467 | .0309 | .0283 | .0833 |
| 4 | .1350 | .0927 | .0875 | .2500 | 14 | .0407 | .0265 | .0239 | .0714 |
| 41/2 | .1211 | .0824 | .0772 | .2222 | 16 | .0363 | .0232 | .0206 | .0625 |
| 5 | .1100 | .0741 | .0689 | .2000 | | | * | | |

MODIFIED SQUARE THREAD



p = pitch in inches

h (basic depth of thread) = 0.5p

H (total depth of thread) = 0.5p + clearance

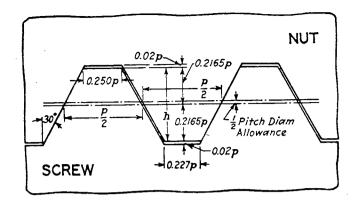
t (thickness of thread) = 0.5p

 F_c (flat at root of screw thread) = 0.4563p - (0.17 × clearance)

F (basic width of flat at crest of screw thread) = 0.4563p

NOTE.—A clearance should be added to "h" to produce extra depth, thus avoiding interference with threads of mating parts at minor or major diameters. The amount of this clearance must be determined from the application of the thread assembly.

| TPI (n) | h+allow. | F | $\mathbf{F}_{\mathtt{c}}$ | p - |
|---------|----------|-------|---------------------------|--------|
| 1 | .5100 | .4563 | .4545 | 1.0000 |
| 1 1/3 | .3850 | .3422 | .3404 | .7500 |
| 1 1/2 | .3433 | .3041 | .3024 | .6666 |
| 1 3/4 | .2957 | .2607 | .2591 | .5714 |
| 2 | .2600 | .2281 | .2264 | .5000 |
| 21/2 | .2100 | .1825 | .1806 | .4000 |
| 3 | .1767 | .1521 | .1503 | .3333 |
| 31/2 | .1528 | .1304 | .1286 | .2857 |
| 4 | .1350 | .1141 | .1123 | .2500 |
| 41/2 | .1211 | .1014 | .0996 | .2222 |
| 5 | .1100 | .0913 | .0895 | .2000 |
| 6 | .0933 | .0761 | .0743 | .1667 |
| 7 | .0814 | .0652 | .0634 | .1429 |
| 8 | .0725 | .0570 | .0553 | .1250 |
| 9 | .0656 | .0507 | .0489 | .1111 |
| 10 | .0600 | .0456 | .0439 | .1000 |
| 11 | .0504 | .0415 | .0406 | .0909 |
| 12 | .0467 | .0380 | .0372 | .0833 |
| 13 | .0435 | .0351 | .0342 | .0769 |
| 14 | .0407 | .0326 | .0317 | .0714 |
| 15 | .0384 | .0304 | .0296 | .0667 |
| 16 | .0363 | .0285 | .0276 | .0625 |



60° STUB THREAD

= pitch in inches

= basic depth of thread = 0.433p

h + = total depth of thread = h + .02p

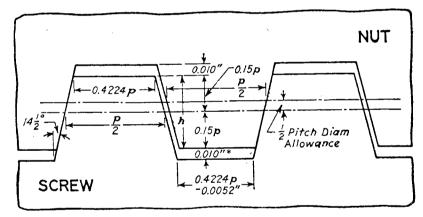
t = thread thickness = .5p

f = width of flat at crest = .250p

Fc = width of flat at root = .227p

n = threads per inch

| TPI(n) | h | h + | F | Fc | р | TPI(n) | h | h + | F | Fc | р |
|--------|-------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|
| 4 | .1083 | .1133 | .0625 | .0567 | .2500 | 9 | .0481 | .0503 | .0278 | .0252 | .1111 |
| 5 | .0866 | .0906 | .0500 | .0454 | .2000 | 10 | .0433 | .0453 | .0250 | .0227 | .1000 |
| 6 | .0722 | .0755 | .0417 | .0378 | .1667 | 12 | .0361 | .0378 | .0208 | .0189 | .0833 |
| 7 | .0619 | .0647 | .0357 | .0324 | .1429 | 14 | .0309 | .0324 | .0179 | .0162 | .0714 |
| . 8 | .0541 | .0566 | .0313 | .0284 | .1250 | .16 | .0271 | .0283 | .0156 | .0142 | .0625 |



29° STUB ACME THREAD

= pitch in inches

= basic depth of thread = .3p

h + = total depth of thread = h + *

t = thread thickness = .5p

F = width of flat at crest = .4224p

Fc = width of flat at root = .4224p-(.52 \times

clearance)

n = threads per inch

| TDI(-) | L I | L 1 | F | Fc | n | TPI(n) | h | h + | F | Fc | р |
|--------|-------|-------|-------|-------|-------|---------|-------|-------|-------|-------|-------|
| TPI(n) | h | h + | r | rc | р | 111(11) | | | | | |
| 2 | .1500 | .1600 | .2112 | .2060 | .5000 | 7 | .0429 | .0529 | .0603 | .0551 | .1429 |
| 21/2 | .1200 | .1300 | .1690 | .1638 | .4000 | 8 | .0375 | .0475 | .0528 | .0476 | .1250 |
| 3 | .1000 | .1100 | .1408 | .1356 | .3333 | 9 | .0333 | .0433 | .0469 | .0417 | .1111 |
| 31/2 | .0857 | .0957 | .1207 | .1155 | .2857 | 10 | .0300 | .0400 | .0422 | .0370 | .1000 |
| 4 | .0750 | .0850 | .1056 | .1004 | .2500 | 12 | .0250 | .0300 | .0352 | .0326 | .0833 |
| 5 | .0600 | .0700 | .0845 | .0793 | .2000 | 14 | .0214 | .0264 | .0302 | .0276 | .0714 |
| 6 | .0500 | .0600 | .0704 | .0652 | .1667 | 16 | .0188 | .0238 | .0264 | .0238 | .0625 |

^{*} A clearance of at least 0.010 in. is added to ''h'' on threads of 10-pitch and coarser, and 0.005 in. on finer pitches, to produce extra depth, thus avoiding interference with threads of mating part at minor or major diameters. It is recognized that there are conditions where a greater or lesser clearance may be desirable.

WHITWORTH FORM THREADS STANDARD SIZES COMMONLY USED

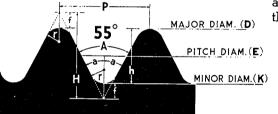
| | Basic Major | | Thread | s per Inch | (British) | |] | Basic Major | | Thread | ls per Inch | (British) | |
|-------|-------------|------------|--------|------------|-------------------|---------------|-------|-------------|------------|--------|-------------|-------------------|-------------------------|
| Diam. | Diam. | Whit. St'd | B.S.F. | Conduit | Admiralty Fine | 26* Series | Diam. | Diam. | Whit. St'd | B.S.F. | Conduit | Admiralty Fine | 26 ³ Seri |
| 1/8 | .1250 | 40 | | | | | 1½ | 1.5000 | 6 | 8 | 14 | 12 | 26 |
| 5/32 | .1562 | 32 | | | | | 15/8 | 1.6250 | 5 | 8 | | 12 | 1 |
| 3/16 | .1875 | 24 | | | 24 | 26 | 13/4 | 1.7500 | 5 | 7 | | 12 | † |
| 7/32 | .2187 | 24 | 28 | | 24 | | 17/8 | 1.8750 | 41/2 | - | | 12 | + |
| 1/4 | .2500 | 20 | 26 | | 24 | 26 | 2 | 2.0000 | 41/2 | 7 | 14 | 8 | 1 |
| 9/32 | .2812 | | 26 | | 24 | | 21/8 | 2.1250 | 41/2 | | | 8 | † |
| 5/16 | .3125 | 18 | 22 | | 24 | 26 | 21/4 | 2.2500 | 4 | 6 | | 8 | |
| 3/8 | .3750 | 16 | 20 | | 24 | 26 | 23/8 | 2.3750 | 4 | | | 8 | 1 |
| 7/16 | .4375 | 14 | 18 | | 24 | 26 | 21/2 | 2.5000 | 4 | 6 | 14 | 8 | <u> </u> |
| 1/2 | .5000 | 12 | 16 | 18 | 20 | 26 | 25/8 | 2.6250 | 4 | | | 8 | \vdash |
| 9/16 | .5625 | 12 | 16 | | 20 | 26 | 23/4 | 2.7500 | 31/2 | 6 | | 8 | † |
| 5/8 | .6250 | 11 | 14 | 18 | 20 | 26 | 27/8 | 2.8750 | 31/2 | , | | 8 | |
| 11/16 | .6875 | 11 | 14 | | 20 | 26 | 3 | 3.0000 | 31/2 | 5 | | 8 | |
| 3/4 | .7500 | 10 | 12 | 16 | 14 | 26 | 31/8 | 3.1250 | 31/2 | | | 8 | |
| 13/16 | .8125 | 10 | 12 | | 14 | 26 | 31/4 | 3.2500 | 31/4 | | | 8 | |
| 7/8 | .8750 | 9 | 11 | | 14 | 26 | 33/8 | 3.3750 | 31/4 | | | 8 | <u> </u> |
| 15/16 | .9375 | 9 | | | 14 | 26 | 31/2 | 3.5000 | 31/4 | | | 8 | |
| 1 | 1.0000 | 8 | 10 | 16 | 12 | 26 | 35/8 | 3.6250 | 31/4 | - | | 8 | — |
| 11/8 | 1.1250 | 7 | 9 | | 12 | 26 | 33/4 | 3.7500 | 3 | - | | 8 | |
| 11/4 | 1.2500 | 7 | 9 | 16 | 12 | 26 | 37/8 | 3.8750 | 3 | | | 8 | <u></u> |
| 1% | 1.3750 | 6 | 8 | | 12 | 26 | 4 | 4.0000 | 3 | | | 6 | _ |

^{*}British Standard Brass Thread.

THREAD DIMENSIONS BRITISH STANDARD (WHITWORTH FORM)

This form of thread is used almost exclusively in Great Britain and extensively in the British Dominions, Asia and South America. There are two standard series, the British Standard Whitworth which is a coarse thread series

and the British Standard Fine. Threads of this form not included in the BSW and BSF series are designated simply Whitworth.

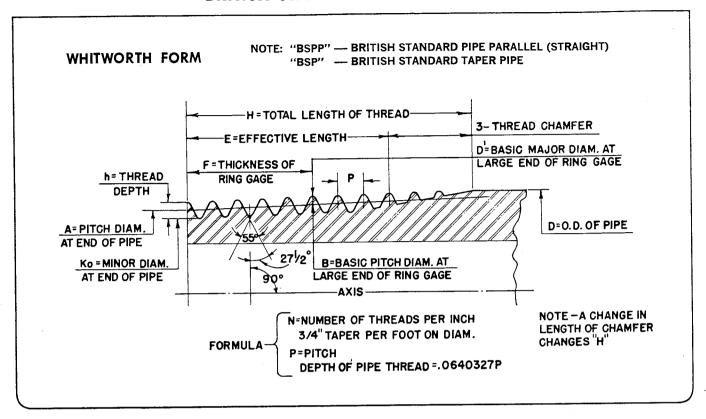


A = 55° = Angle of thread
a = 27½° = ½ Angle of thread
f = 1/6H = Depth of truncation
H = 0.960491p = Depth Theoretical V 55° thread
h = 0.640327p, or 4/6H = Depth Whitworth form thread

n = Number threads per inch
p = 1/n = Pitch
r = 0.137329p = Radius of crest and root

| n | h | r | р | n | h | r | р | n | h | T - | · |
|-------|-------|--------------|-------|----|-------|-------|-------|-----|-------|-------|-------|
| | | | - | | | - | Р | 111 | 11 | r | q |
| 21/4 | .2846 | .0610 | .4444 | 9 | .0711 | .0153 | .1111 | 34 | .0188 | .0040 | .0294 |
| 23/8 | .2696 | .0578 | .4210 | 10 | .0640 | .0137 | .1000 | 36 | .0178 | .0038 | .0278 |
| 21/2 | .2561 | .0549 | .4000 | 11 | .0582 | .0125 | .0909 | 38 | .0169 | .0036 | .0263 |
| 25/8 | .2439 | .0523 | .3810 | 12 | .0534 | .0114 | .0833 | 40 | .0160 | .0034 | .0250 |
| 23/4 | .2328 | .0499 | .3636 | 13 | .0493 | .0106 | .0769 | 42 | .0152 | .0033 | .0238 |
| 2 1/8 | .2227 | .0478 | .3478 | 14 | .0457 | .0098 | .0714 | 44 | .0146 | .0031 | .0227 |
| 3 | .2134 | .0458 | .3333 | 15 | .0427 | .0092 | .0667 | 46 | .0139 | .0030 | .0217 |
| 31/4 | .1970 | .0422 | .3077 | 16 | .0400 | .0086 | .0625 | 48 | .0133 | .0029 | .0208 |
| 31/2 | .1830 | .0392 | .2857 | 18 | .0356 | .0076 | .0556 | 50 | .0128 | .0027 | .0200 |
| 4 | .1601 | .0343 | .2500 | 20 | .0320 | .0069 | .0500 | 52 | .0123 | .0026 | .0192 |
| 41/4 | .1423 | .0305 | .2222 | 22 | .0291 | .0062 | .0455 | 56 | .0114 | .0025 | .0179 |
| 5 | .1281 | .0275 | .2000 | 24 | .0267 | .0057 | .0417 | 60 | .0107 | .0023 | .0167 |
| 5½ | .1164 | .0250 | .1818 | 26 | .0246 | .0053 | .0385 | 64 | .0100 | .0021 | .0156 |
| 6 | .1067 | .0229 | .1667 | 28 | .0229 | .0049 | .0357 | 68 | .0094 | .0020 | .0147 |
| 7 | .0915 | .0196 | .1429 | 30 | .0213 | .0046 | .0333 | 72 | .0089 | .0019 | .0139 |
| 8 | .0800 | .0172 | .1250 | 32 | .0200 | .0043 | .0313 | 80 | .0080 | .0017 | .0125 |

BRITISH STANDARD PIPE THREADS

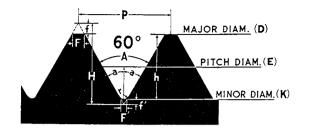


BASIC THREAD DIMENSIONS BRITISH STANDARD PIPE THREAD

| Pipe Size Nominal—Inches | Threads per Inch | Outside Diameter of Pipe (Mean)— Inches | Pitch Inches | Depth of Thread .064032 P—Inches | Basic Major Diam. at Large End of Ring Gage— Inches | Basic Pitch Diam. at Large End of Ring Gage— Inches | Pitch Diam. at End of Pipe— Inches | Minor Diam. at End of Pipe— Inches | Thickness of Ring Gage = Normal Engagement by Hand—Inches | Effective Length of Thread (Basic)— Inches | Total Length of Thread—Inches | Tolera Leng | Minus nce on the of gement Inches | Tap Drill Sizes— Inches |
|-----------------------------|------------------|---|--------------|-------------------------------------|--|---|--|--|--|--|----------------------------------|----------------|---|----------------------------|
| | N | D | P | h | D1 | В | A | Ko | F | E | H | | <u> </u> | |
| 1/8 | 28 | .400 | .03571 | .0229 | .383 | .3601 | .3503 | 3274_ | .1563 | .2545 | .362 | .0357 | .0446 | 21/64 |
| 1/4 | 19 | .538 | .05263 | .0337 | .518 | .4843 | .4695 | .4358 | .2367 | .3814 | .539 | .0526 | .0658 | 29/64 |
| 3/8 | 19 | .676 | .05263 | .0337 | .656 | .6223 | .6067 | .5730 | .2500 | .3947 | .553 | .0526 | .0658 | 37/64 |
| 1/2 | 14 | .847 | .07143 | .0457 | .825 | .7793 | .7592 | .7135 | .3214 | .5178 | .732 | .0714 | .0893 | 23/32 |
| 3/4 | 14 | 1.063 | .07143 | .0457 | 1.041 | .9953 | .9719 | .9262 | .3750 | .5714 | .786 | .0714 | .0893 | 59/64 |
| 1 | 11 | 1.336 | .09091 | .0582 | 1.309 | 1.2508 | 1.2253 | 1.1671 | .4091 | .6591 | .932 | .0909 | .1136 | 111/64 |
| 11/4 | 11 | 1.677 | .09091 | .0582 | 1.650 | 1.5918 | 1.5605 | 1.5023 | .5000 | .7500 | 1.023 | .0909 | .1136 | 11/2 |
| 11/2 | 11 | 1.909 | .09091 | .0582 | 1.882 | 1.8238 | 1.7925 | 1.7343 | .5000 | 7500 | 1.023 | .0909 | .1136 | 13/4 |
| 2 | 11 | 2.381 | .09091 | .0582 | 2.347 | 2.2888 | 2.2497 | 2.1915 | .6250 | .9204 | 1.193 | .0909 | .1136 | 27/32 |
| 21/2 | 11 | 2.996 | .09091 | .0582 | 2.960 | 2.9018 | 2.8588 | 2.8006 | .6875 | 1.0511 | 1.324 | .1364 | .1364 | 213/16 |
| 3 | 11 | 3.499 | .09091 | .0582 | 3.460 | 3.4018 | 3.3510 | 3.2928 | .8125 | 1.1761 | 1.449 | .1364 | .1364 | 35,16 |
| 31/2 | 11 | 3.991 | .09091 | .0582 | 3.950 | 3.8918 | 3.8371 | 3.7789 | .8750 | 1.2386 | 1.511 | .1364 | .1364 | 313/16 |
| 4 | 11 | 4.494 | .09091 | .0582 | 4.450 | 4.3918 | 4.3293 | 4.2711 | 1.0000 | 1.4091 | 1.682 | .1364 | .1364 | . |
| 5 | | 5.498 | .09091 | .0582 | 5.450 | 5.3918 | 5.3215 | 5.2633 | 1.1250 | 1.5795 | 1.852 | .1364 | .1364 | _ |
| 6 | 11 | 6.501 | .09091 | .0582 | 6.450 | 6.3918 | 6.3215 | 6.2633 | 1.1250 | 1.5795 | 1.852 | .1364 | .1364 | l |
| 7 | 10 | 7.519 | .10000 | .0640 | 7.450 | 7.3860 | 7.3001 | 7.2361 | 1.3750 | 1.9250 | 2.225 | .2000 | .2000 | <u> </u> |
| 8 | 10 | 8.524 | .10000 | .0640 | 8.450 | 8.3860 | 8.2922 | 8.2282 | 1.5000 | 2.0500 | 2.3500 | .2000 | .2000 | |
| 9 | 10 | 9.529 | .10000 | .0640 | 9.450 | 9.3860 | 9.2922 | 9.2282 | 1.5000 | 2.0500 | 2.3500 | .2000 | .2000 | |
| 10 | 10 | 10.534 | .10000 | .0640 | 10.450 | 10.3860 | 10.2844 | 10.2204 | 1.6250 | 2.1750 | 2.4750 | .2000 | .2000 | |
| 11 | 8 | 11.540 | .12500 | .0800 | 11.450 | 11.3700 | 11.2684 | 11.1884 | 1.6250 | 2.3125 | 2.688 | .2500 | .2500 | |
| 12 | 8 | 12.545 | .12500 | .0800 | 12.450 | 12.3700 | 12.2684 | 12.1884 | 1.6250 | 2.3125 | 2.688 | .2500 | .2500 | $oldsymbol{\perp}$ |

THREAD DIMENSIONS . METRIC

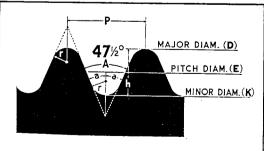
METRIC STANDARD



A = 60° = Angle of thread
a = 30° = ½ Angle of thread
F = ½p = Flat at crest
F' = ½fg = Flat at root
f = ½fH = Depth of truncation at crest
f' = ½fH = Depth of truncation at root
H = 0.866025p = Depth of theoretical sharp V thread
h = 0.70365p, or 13½fH = Depth Metric form thread
p = Pitch
r = Radius of root

| | q | h | F | | | þ | , | P | |
|------|----------|-------|-------|-------|------|--------|-------|-------|---------|
| MM | Inches | 11 | F | r | MM | Inches | h h | F | r |
| .35 | .0138 | .0096 | .0017 | .0008 | 1.8 | .0709 | .0496 | .0089 | .0041 |
| .40 | .0158 | .0110 | .0020 | .0009 | 1.9 | .0748 | .0524 | .0093 | .0043 |
| .45 | .0177 | .0124 | .0022 | .0010 | 2.0 | .0787 | .0551 | .0098 | .0046 |
| .50 | .0197 | .0138 | .0025 | .0011 | 2.25 | .0886 | .0620 | .0111 | .0051 |
| .55 | .0217 | .0152 | .0027 | .0013 | 2.5 | .0984 | .0689 | .0123 | .0057 |
| .60 | .0236 | .0165 | .0030 | .0014 | 2.75 | .1083 | .0758 | .0135 | .0063 |
| .65 | .0256 | .0179 | .0032 | .0015 | 3.0 | .1181 | .0827 | .0148 | .0068 |
| .70 | .0276 | .0193 | .0034 | .0016 | 3.25 | .1280 | .0896 | .0160 | .0074 |
| .75 | .0295 | .0207 | .0037 | .0017 | 3.5 | .1378 | .0964 | .0172 | .0080 |
| .80 | .0315 | .0220 | .0039 | .0018 | 3.75 | .1476 | .1033 | .0185 | .0086 |
| .85 | .0335 | .0234 | .0042 | .0019 | 4.0 | .1575 | .1102 | .0197 | .0092 |
| .90 | .0354 | .0248 | .0044 | .0021 | 4.5 | .1772 | .1240 | .0221 | .0103 |
| .95 | .0374 | .0262 | .0047 | .0022 | 5.0 | .1969 | .1378 | .0246 | .0114 |
| 1.0 | .0394 | .0276 | .0049 | .0023 | 5.5 | .2165 | .1516 | .0271 | .0126 |
| 1.1 | .0433 | .0303 | .0054 | .0025 | 6.0 | .2362 | .1654 | .0295 | .0137 |
| 1.2 | .0472 | .0331 | .0059 | .0027 | 6.5 | .2559 | .1791 | .0320 | .0148 |
| 1.25 | .0492 | .0344 | .0061 | .0029 | 7.0 | .2756 | .1929 | .0344 | .0160 |
| 1.3 | .0512 | .0359 | .0064 | .0030 | 7.5 | .2953 | .2067 | .0369 | .0171 - |
| 1.4 | .0551 | .0386 | .0069 | .0032 | 8.0 | .3150 | .2205 | .0394 | .0183 |
| 1.5 | .0591 | .0413 | .0074 | .0034 | 8.5 | .3346 | .2342 | .0418 | .0194 |
| 1.6 | .0630 | .0441 | .0079 | .0037 | 9.0 | .3543 | .2480 | .0443 | .0206 |
| 1.7 | .0669 | .0468 | .0084 | .0039 | 9.5 | .3740 | .2618 | .0467 | .0217 |
| 1.75 | .0689 | .0482 | .0086 | .0040 | 10.0 | .3937 | .2756 | .0492 | .0228 |

BRITISH ASSOCIATION STANDARD



A = 47½° = Angle of thread a = 23¾° = ½ Angle of thread h = 0.600p = Depth British Association Thread

p = Pitch r = 2 11p = Radius of crest and root

| British | Diam | neter | Pi | tch | 1. | |
|-----------|------|--------|-----|--------|-------|-------|
| Asso. No. | MM | Inches | MM | Inches | h | r |
| 0 | 6.0 | .236 | 1.0 | .03937 | .0236 | .0072 |
| 1 | 5.3 | .209 | .9 | .03543 | .0213 | .0064 |
| 2 | 4.7 | .185 | .81 | .03189 | .0191 | .0058 |
| 3 | 4.1 | .161 | .73 | .02874 | .0172 | .0052 |
| 4 | 3.6 | .142 | .66 | .02598 | .0156 | .0047 |
| 5 | 3.2 | .126 | .59 | .02323 | .0139 | .0042 |
| 6 | 2.8 | .110 | .53 | .02087 | .0125 | .0038 |
| 7 | 2.5 | .098 | .48 | .01890 | .0113 | .0034 |
| 8 | 2.2 | .087 | .43 | .01693 | .0102 | .0031 |
| 9 | 1.9 | .075 | .39 | .01535 | .0092 | .0028 |
| 10 | 1.7 | .067 | .35 | .01378 | .0083 | .0025 |

rabies.

DECIMAL EQUIVALENTS OF MILLIMETERS

FROM 1/10 TO 100 MM ADVANCING BY 1/10 MILLIMETERS

| MM | Inches | MM | Inches | MM | Inches | ММ | Inches | ММ | Inches | ММ | Inches | MM | Inches |
|----------------------|--|---------------------------------|--|--------------------------------------|--|--------------------------------------|--|--------------------------------------|---|--------------------------------------|---|--------------------------------------|---|
| .1 | .00394 | 7.6 | .29921 | 15.1 | .59488 | 22.6 | .88976 | 30.1 | 1.18503 | 37.6 | 1.48031 | 45.1 | 1.77558 |
| .2 | .00787 | 7.7 | .30314 | 15.2 | .59842 | 22.7 | .89369 | 30.2 | 1.18897 | 37.7 | 1.48424 | 45.2 | 1.77952 |
| .3 | .01181 | 7.8 | .30708 | 15.3 | .60236 | 22.8 | .89763 | 30.3 | 1.19291 | 37.8 | 1.48818 | 45.3 | 1.78346 |
| .4 | .01575 | 7.9 | .31102 | 15.4 | .60629 | 22.9 | .90157 | 30.4 | 1.19684 | 37.9 | 1.49212 | 45.4 | 1.78739 |
| .5 | .01968 | 8.0 | .31496 | 15.5 | .61023 | 23.0 | .90551 | 30.5 | 1.20078 | 38.0 | 1.49606 | 45.5 | 1.79133 |
| .6 .7 .8 .9 | .02362 .02756 .03149 .03543 .03937 | 8.1 8.2 8.3 8.4 8.5 | .31889 .32283 .32677 .33070 .33464 | 15.6 15.7 15.8 15.9 16.0 | .61417 .61810 .62204 .62598 .62992 | 23.1 23.2 23.3 23.4 23.5 | .90944 .91338 .91732 .92125 .92519 | 30.6 30.7 30.8 30.9 31.0 | 1.20472 1.20865 1.21259 1.21653 1.22047 | 38.1 38.2 38.3 38.4 38.5 | 1.49999 1.50393 1.50787 1.51180 1.51574 | 45.6 45.7 45.8 45.9 46.0 | 1.79527 1.79920 1.80314 1.80708 1.81102 |
| 1.1 | .04330 | 8.6 | .33858 | 16.1 | .63385 | 23.6 | .92913 | 31.1 | 1.22440 | 38.6 | 1.51968 | 46.1 | 1.81495 |
| 1.2 | .04724 | 8.7 | .34251 | 16.2 | .63779 | 23.7 | .93306 | 31.2 | 1.22834 | 38.7 | 1.52361 | 46.2 | 1.81889 |
| 1.3 | .05118 | 8.8 | .34645 | 16.3 | .64173 | 23.8 | .93700 | 31.3 | 1.23228 | 38.8 | 1.52755 | 46.3 | 1.82283 |
| 1.4 | .05512 | 8.9 | .35039 | 16.4 | .64566 | 23.9 | .94094 | 31.4 | 1.23621 | 38.9 | 1.53149 | 46.4 | 1.82676 |
| 1.5 | .05905 | 9.0 | .35433 | 16.5 | .64960 | 24.0 | .94488 | 31.5 | 1.24015 | 39.0 | 1.53543 | 46.5 | 1.83070 |
| 1.6 | .06299 | 9.1 | .35826 | 16.6 | .65354 | 24.1 | .94881 | 31.6 | 1.24409 | 39.1 | 1.53936 | 46.6 | 1.83464 |
| 1.7 | .06692 | 9.2 | .36220 | 16.7 | .65747 | 24.2 | .95275 | 31.7 | 1.24802 | 39.2 | 1.54330 | 46.7 | 1.83857 |
| 1.8 | .07086 | 9.3 | .36614 | 16.8 | .66141 | 24.3 | .95669 | 31.8 | 1.25196 | 39.3 | 1.54724 | 46.8 | 1.84251 |
| 1.9 | .07480 | 9.4 | .37007 | 16.9 | .66535 | 24.4 | .96062 | 31.9 | 1.25590 | 39.4 | 1.55117 | 46.9 | 1.84645 |
| 2.0 | .07874 | 9.5 | .37401 | 17.0 | .66929 | 24.5 | .96456 | 32.0 | 1.25984 | 39.5 | 1.55511 | 47.0 | 1.85039 |
| 2.1 | .08267 | 9.6 | .37795 | 17.1 | .67322 | 24.6 | .96850 | 32.1 | 1.26377 | 39.6 | 1.55905 | 47.1 | 1.85432 |
| 2.2 | .08661 | 9.7 | .38188 | 17.2 | .67716 | 24.7 | .97243 | 32.2 | 1.26771 | 39.7 | 1.56298 | 47.2 | 1.85826 |
| 2.3 | .09055 | 9.8 | .38582 | 17.3 | .68110 | 24.8 | .97637 | 32.3 | 1.27165 | 39.8 | 1.56692 | 47.3 | 1.86220 |
| 2.4 | .09448 | 9.9 | .38976 | 17.4 | .68503 | 24.9 | .98031 | 32.4 | 1.27558 | 39.9 | 1.57086 | 47.4 | 1.86613 |
| 2.5 | .09842 | 10.0 | .39370 | 17.5 | .68897 | 25.0 | .98425 | 32.5 | 1.27952 | 40.0 | 1.57480 | 47.5 | 1.87007 |
| 2.6 | .10236 | 10.1 | .39763 | 17.6 | .69291 | 25.1 | .98818 | 32.6 | 1.28346 | 40.1 | 1.57873 | 47.6 | 1.87401 |
| 2.7 | .10629 | 10.2 | .40157 | 17.7 | .69684 | 25.2 | .99212 | 32.7 | 1.28749 | 40.2 | 1.58267 | 47.7 | 1.87794 |
| 2.8 | .11023 | 10.3 | .40551 | 17.8 | .70078 | 25.3 | .99606 | 32.8 | 1.29133 | 40.3 | 1.58661 | 47.8 | 1.88188 |
| 2.9 | .11417 | 10.4 | .40944 | 17.9 | .70472 | 25.4 | .99999 | 32.9 | 1.29527 | 40.4 | 1.59054 | 47.9 | 1.88582 |
| 3.0 | .11811 | 10.5 | .41338 | 18.0 | .70866 | 25.5 | 1.00393 | 33.0 | 1.29921 | 40.5 | 1.59448 | 48.0 | 1.88976 |
| 3.1 | .12204 | 10.6 | .41732 | 18.1 | .71259 | 25.6 | 1.00787 | 33.1 | 1.30314 | 40.6 | 1.59842 | 48.1 | 1.89369 |
| 3.2 | .12598 | 10.7 | .42125 | 18.2 | .71653 | 25.7 | 1.01180 | 33.2 | 1.30708 | 40.7 | 1.60235 | 48.2 | 1.89763 |
| 3.3 | .12992 | 10.8 | .42519 | 18.3 | .72047 | 25.8 | 1.01574 | 33.3 | 1.31102 | 40.8 | 1.60629 | 48.3 | 1.90157 |
| 3.4 | .13385 | 10.9 | .42913 | 18.4 | .72440 | 25.9 | 1.01968 | 33.4 | 1.31495 | 40.9 | 1.61023 | 48.4 | 1.90550 |
| 3.5 | .13779 | 11.0 | .43307 | 18.5 | .72834 | 26.0 | 1.02362 | 33.5 | 1.31889 | 41.0 | 1.61417 | 48.5 | 1.90944 |
| 3.6 | .14173 ⁻ | 11.1 | .43700 | 18.6 | .73228 | 26.1 | 1.02755 | 33.6 | 1.32283 | 41.1 | 1.61810 | 48.6 | 1.91338 |
| 3.7 | .14566 | 11.2 | .44094 | 18.7 | .73621 | 26.2 | 1.03149 | 33.7 | 1.32676 | 41.2 | 1.62204 | 48.7 | 1.91731 |
| 3.8 | .14960 | 11.3 | .44488 | 18.8 | .74015 | 26.3 | 1.03543 | 33.8 | 1.33070 | 41.3 | 1.62598 | 48.8 | 1.92125 |
| 3.9 | .15354 | 11.4 | .44881 | 18.9 | .74409 | 26.4 | 1.03936 | 33.9 | 1.33464 | 41.4 | 1.62991 | 48.9 | 1.92519 |
| 4.0 | .15748 | 11.5 | .45275 | 19.0 | .74803 | 26.5 | 1.04330 | 34.0 | 1.33858 | 41.5 | 1.63385 | 49.0 | 1.92913 |
| 4.1 | .16141 | 11.6 | .45669 | 19.1 | .75196 | 26.6 | 1.04724 | 34.1 | 1.34251 | 41.6 | 1.63779 | 49.1 | 1.93306 |
| 4.2 | .16535 | 11.7 | .46062 | 19.2 | .75590 | 26.7 | 1.05117 | 34.2 | 1.34645 | 41.7 | 1.64172 | 49.2 | 1.93700 |
| 4.3 | .16929 | 11.8 | .46456 | 19.3 | .75984 | 26.8 | 1.05511 | 34.3 | 1.35039 | 41.8 | 1.64566 | 49.3 | 1.94094 |
| 4.4 | .17322 | 11.9 | .46850 | 19.4 | .76377 | 26.9 | 1.05905 | 34.4 | 1.35432 | 41.9 | 1.64960 | 49.4 | 1.94487 |
| 4.5 | .17716 | 12.0 | .47244 | 19.5 | .76771 | 27.0 | 1.06299 | 34.5 | 1.35826 | 42.0 | 1.65354 | 49.5 | 1.94881 |
| 4.6 | .18110 | 12.1 | .47637 | 19.6 | .77165 | 27.1 | 1.06692 | 34.6 | 1.36220 | 42.1 | 1.65747 | 49.6 | 1.95275 |
| 4.7 | .18503 | 12.2 | .48031 | 19.7 | .77558 | 27.2 | 1.07086 | 34.7 | 1.36613 | 42.2 | 1.66141 | 49.7 | 1.95668 |
| 4.8 | .18897 | 12.3 | .48425 | 19.8 | .77952 | 27.3 | 1.07480 | 34.8 | 1.37007 | 42.3 | 1.66535 | 49.8 | 1.96062 |
| 4.9 | .19291 | 12.4 | .48818 | 19.9 | .78346 | 27.4 | 1.07873 | 34.9 | 1.37401 | 42.4 | 1.66928 | 49.9 | 1.96456 |
| 5.0 | .19685 | 12.5 | .49212 | 20.0 | .78740 | 27.5 | 1.08267 | 35.0 | 1.37795 | 42.5 | 1.67322 | 50.0 | 1.96850 |
| 5.1 | .20078 | 12.6 | .49606 | 20.1 | .79133 | 27.6 | 1.08661 | 35.1 | 1.38188 | 42.6 | 1.67716 | 50.1 | 1.97243 |
| 5.2 | .20472 | 12.7 | .49999 | 20.2 | .79527 | 27.7 | 1.09054 | 35.2 | 1.38582 | 42.7 | 1.68109 | 50.2 | 1.97637 |
| 5.3 | .20866 | 12.8 | .50393 | 20.3 | .79921 | 27.8 | 1.09448 | 35.3 | 1.38976 | 42.8 | 1.68503 | 50.3 | 1.98031 |
| 5.4 | .21259 | 12.9 | .50787 | 20.4 | .80314 | 27.9 | 1.09842 | 35.4 | 1.39369 | 42.9 | 1.68897 | 50.4 | 1.98424 |
| 5.5 | .21653 | 13.0 | .51181 | 20.5 | .80708 | 28.0 | 1.10236 | 35.5 | 1.39763 | 43.0 | 1.69291 | 50.5 | 1.98818 |
| 5.6 | .22047 | 13.1 | .51574 | 20.6 | .81102 | 28.1 | 1.10629 | 35.6 | 1.40157 | 43.1 | 1.69684 | 50.6 | 1.99212 |
| 5.7 | .22440 | 13.2 | .51968 | 20.7 | .81495 | 28.2 | 1.11023 | 35.7 | 1.40550 | 43.2 | 1.70078 | 50.7 | 1.99605 |
| 5.8 | .22834 | 13.3 | .52362 | 20.8 | .81889 | 28.3 | 1.11417 | 35.8 | 1.40944 | 43.3 | 1.70472 | 50.8 | 1.99999 |
| 5.9 | .23228 | 13.4 | .52755 | 20.9 | .82283 | 28.4 | 1.11810 | 35.9 | 1.41338 | 43.4 | 1.70865 | 50.9 | 2.00393 |
| 6.0 | .23622 | 13.5 | .53149 | 21.0 | .82677 | 28.5 | 1.12204 | 36.0 | 1.41732 | 43.5 | 1.71259 | 51.0 | 2.00787 |
| 6.1 | .24015 | 13.6 | .53543 | 21.1 | .83070 | 28.6 | 1.12598 | 36.1 | 1.42125 | 43.6 | 1.71653 | 51.1 | 2.01180 |
| 6.2 | .24409 | 13.7 | .53936 | 21.2 | .83464 | 28.7 | 1.12991 | 36.2 | 1.42519 | 43.7 | 1.72046 | 51.2 | 2.01574 |
| 6.3 | .24803 | 13.8 | .54330 | 21.3 | .83858 | 28.8 | 1.13385 | 36.3 | 1.42913 | 43.8 | 1.72440 | 51.3 | 2.01968 |
| 6.4 | .25196 | 13.9 | .54724 | 21.4 | .84251 | 28.9 | 1.13779 | 36.4 | 1.43306 | 43.9 | 1.72834 | 51.4 | 2.02361 |
| 6.5 | .25590 | 14.0 | .55118 | 21.5 | .84645 | 29.0 | 1.14173 | 36.5 | 1.43700 | 44.0 | 1.73228 | 51.5 | 2.02755 |
| 6.6 | .25984 | 14.1 | .55511 | 21.6 | .85039 | 29.1 | 1.14566 | 36.6 | 1.44094 | 44.1 | 1.73621 | 51.6 | 2.03149 |
| 6.7 | .26377 | 14.2 | .55905 | 21.7 | .85432 | 29.2 | 1.14960 | 36.7 | 1.44487 | 44.2 | 1.74015 | 51.7 | 2.03542 |
| 6.8 | .26771 | 14.3 | .56299 | 21.8 | .85826 | 29.3 | 1.15354 | 36.8 | 1.44881 | 44.3 | 1.74409 | 51.8 | 2.03936 |
| 6.9 | .27165 | 14.4 | .56692 | 21.9 | .86220 | 29.4 | 1.15747 | 36.9 | 1.45275 | 44.4 | 1.74802 | 51.9 | 2.04330 |
| 7.0 | .27559 | 14.5 | .57086 | 22.0 | .86614 | 29.5 | 1.16141 | 37.0 | 1.45669 | 44.5 | 1.75196 | 52.0 | 2.04724 |
| 7.1 | .27952 | 14.6 | .57480 | 22.1 | .87007 | 29.6 | 1.16535 | 37.1 | 1.46062 | 44.6 | 1.75590 | 52.1 | 2.05117 |
| 7.2 | .28346 | 14.7 | .57873 | 22.2 | .87401 | 29.7 | 1.16928 | 37.2 | 1.46456 | 44.7 | 1.75983 | 52.2 | 2.05511 |
| 7.3 | .28740 | 14.8 | .58267 | 22.3 | .87795 | 29.8 | 1.17322 | 37.3 | 1.46850 | 44.8 | 1.76337 | 52.3 | 2.05905 |
| 7.4 | .29133 | 14.9 | .58661 | 22.4 | .88188 | 29.9 | 1.17716 | 37.4 | 1.47243 | 44.9 | 1.76771 | 52.4 | 2.06298 |
| 7.5 | .29527 | 15.0 | .59055 | 22.5 | .88582 | 30.0 | 1.18110 | 37.5 | 1.47637 | 45.0 | 1.77165 | 52.5 | 2.06692 |

| | | | - | | | | | | | | |
|------------------------------|--|------------------------------|--|------------------------------|--|------------------------------|--|------------------------------|--|---------------------------------------|---|
| MM | Inches | MM | Inches | MM | Inches | MM | Inches | ММ | Inches | ММ | Inches |
| 52.6 | 2.07086 | 60.5 | 2.38188 | 68.4 | 2.69290 | 76.3 | 3.00393 | 84.2 | 3.31495 | 92.1 | 3.62597 |
| 52.7 | 2.07479 | 60.6 | 2.38582 | 68.5 | 2.69684 | 76.4 | 3.00780 | 84.3 | 3.31889 | 92.2 | 3.62991 |
| 52.8 | 2.07873 | 60.7 | 2.38975 | 68.6 | 2.70078 | 76.5 | 3.01180 | 84.4 | 3.32282 | 92.3 | 3.63385 |
| 52.9 | 2.08267 | 60.8 | 2.39369 | 68.7 | 2.70471 | 76.6 | 3.01574 | 84.5 | 3.32676 | 92.4 | 3.63778 |
| 53.0 | 2.08661 | 60.9 | 2.39763 | 68.8 | 2.70865 | 76.7 | 3.01967 | 84.6 | 3.33070 | 92.5 | 3.64172 |
| 53.1 | 2.09054 | 61.0 | 2.40157 | 68.9 | 2.71259 | 76.8 | 3.02361 | 84.7 | 3.33463 | 92.6 | 3.64566 |
| 53.2 | 2.09448 | 61.1 | 2.40550 | 69.0 | 2.71653 | 76.9 | 3.02755 | 84.8 | 3.33857 | 92.7 | 3.64959 |
| 53.3 | 2.09842 | 61.2 | 2.40944 | 69.1 | 2.72046 | 77.0 | 3.03149 | 84.9 | 3.34251 | 92.8 | 3.65353 |
| 53.4 | 2.10235 | 61.3 | 2.41388 | 69.2 | 2.72440 | 77.1 | 3.03542 | 85.0 | 3.34645 | 92.9 | 3.65747 |
| 53.5 | 2.10629 | 61.4 | 2.41731 | 69.3 | 2.72834 | 77.2 | 3.03936 | 85.1 | 3.35038 | 93.0 | 3.66141 |
| 53.6 | 2.11023 | 61.5 | 2.42125 | 69.4 | 2.73227 | 77.3 | 3.04330 | 85.2 | 3.35432 | 93.1 | 3.66534 |
| 53.7 | 2.11416 | 61.6 | 2.42519 | 69.5 | 2.73621 | 77.4 | 3.04723 | 85.3 | 3.35826 | 93.2 | 3.66928 |
| 53.8 | 2.11810 | 61.7 | 2.42912 | 69.6 | 2.74015 | 77.5 | 3.05117 | 85.4 | 3.36219 | 93.3 | 3.67322 |
| 53.9 | 2.12204 | 61.8 | 2.43306 | 69.7 | 2.74408 | 77.6 | 3.05511 | 85.5 | 3.36613 | 93.4 | 3.67715 |
| 54.0 | 2.12598 | 61.9 | 2.43700 | 69.8 | 2.74802 | 77.7 | 3.05904 | 85.6 | 3.37007 | 93.5 | 3.68109 |
| 54.1 | 2.12991 | 62.0 | 2.44094 | 69.9 | 2.75196 | 77.8 | 3.06298 | 85.7 | 3.37400 | 93.6 | 3.68503 |
| 54.2 | 2.13385 | 62.1 | 2.44487 | 70.0 | 2.75590 | 77.9 | 3.06692 | 85.8 | 3.37794 | 93.7 | 3.68896 |
| 54.3 | 2.13779 | 62.2 | 2.44881 | 70.1 | 2.75983 | 78.0 | 3.07086 | 85.9 | 3.38188 | 93.8 | 3.69290 |
| 54.4 | 2.14172 | 62.3 | 2.45275 | 70.2 | 2.76377 | 78.1 | 3.07479 | 86.0 | 3.38582 | 93.9 | 3.69684 |
| 54.5 | 2.14566 | 62.4 | 2.45668 | 70.3 | 2.76771 | 78.2 | 3.07873 | 86.1 | 3.38975 | 94.0 | 3.70078 |
| 54.6 | 2.14960 | 62.5 | 2.46062 | 70.4 | 2.77164 | 78.3 | 3.08267 | 86.2 | 3.39369 | 94.1 | 3.70471 |
| 54.7 | 2.15353 | 62.6 | 2.46456 | 70.5 | 2.77558 | 78.4 | 3.08660 | 86.3 | 3.39736 | 94.2 | 3.70865 |
| 54.8 | 2.15747 | 62.7 | 2.46849 | 70.6 | 2.77952 | 78.5 | 3.09054 | 86.4 | 3.40156 | 94.3 | 3.71259 |
| 54.9 | 2.16141 | 62.8 | 2.47243 | 70.7 | 2.78345 | 78.6 | 3.09448 | 86.5 | 3.40550 | 94.4 | 3.71652 |
| 55.0 | 2.16535 | 62.9 | 2.47637 | 70.8 | 2.78739 | 78.7 | 3.09841 | 86.6 | 3.40944 | 94.5 | 3.72046 |
| 55.1 | 2.16928 | 63.0 | 2.48031 | 70.9 | 2.79133 | 78.8 | 3.10235 | 86.7 | 3.41337 | 94.6 | 3.72440 |
| 55.2 | 2.17322 | 63.1 | 2.48424 | 71.0 | 2.79527 | 78.9 | 3.10629 | 86.8 | 3.41731 | 94.7 | 3.72833 |
| 55.3 | 2.17716 | 63.2 | 2.48818 | 71.1 | 2.79920 | 79.0 | 3.11023 | 86.9 | 3.42125 | 94.8 | 3.73227 |
| 55.4 | 2.18109 | 63.3 | 2.49212 | 71.2 | 2.80314 | 79.1 | 3.11416 | 87.0 | 3.42519 | 94.9 | 3.73621 |
| 55.5 | 2.18503 | 63.4 | 2.49605 | 71.3 | 2.80708 | 79.2 | 3.11810 | 87.1 | 3.42912 | 95.0 | 3.74015 |
| 55.6 | 2.18897 | 63.5 | 2.49999 | 71.4 | 2.81101 | 79.3 | 3.12204 | 87.2 | 3.43306 | 95.1 | 3.74408 |
| 55.7 | 2.19290 | 63.6 | 2.50393 | 71.5 | 2.81495 | 79.4 | 3.12597 | 87.3 | 3.43700 | 95.2 | 3.74802 |
| 55.8 | 2.19684 | 63.7 | 2.50786 | 71.6 | 2.81889 | 79.5 | 3.12991 | 87.4 | 3.44093 | 95.3 | 3.75196 |
| 55.9 | 2.20078 | 63.8 | 2.51180 | 71.7 | 2.82282 | 79.6 | 3.13385 | 87.5 | 3.44487 | 95.4 | 3.75589 |
| 56.0 | 2.20472 | 63.9 | 2.51574 | 71.8 | 2.82676 | 79.7 | 3.13778 | 87.6 | 3.44881 | 95.5 | 3.75983 |
| 56.1 | 2.20865 | 64.0 | 2.51968 | 71.9 | 2.83070 | 79.8 | 3.14172 | 87.7 | 3.45274 | 95.6 | 3.76377 |
| 56.2 | 2.21259 | 64.1 | 2.52361 | 72.0 | 2.83464 | 79.9 | 3.14566 | 87.8 | 3.45668 | 95.7 | 3.76770 |
| 56.3 | 2.21653 | 64.2 | 2.52755 | 72.1 | 2.83857 | 80.0 | 3.14960 | 87.9 | 3.46062 | 95.8 | 3.77164 |
| 56.4 | 2.22096 | 64.3 | 2.53149 | 72.2 | 2.84251 | 80.1 | 3.15353 | 88.0 | 3.46456 | 95.9 | 3.77558 |
| 56.5 | 2.22440 | 64.4 | 2.53542 | 72.3 | 2.84645 | 80.2 | 3.15747 | 88.1 | 3.46849 | 96.0 | 3.77952 |
| 56.6 | 2.22834 | 64.5 | 2.53936 | 72.4 | 2.85038 | 80.3 | 3.16141 | 88.2 | 3.47243 | 96.1 | 3.78345 |
| 56.7 | 2.23227 | 64.6 | 2.54330 | 72.5 | 2.85432 | 80.4 | 3.16534 | 88.3 | 3.47637 | 96.2 | 3.78739 |
| 56.8 | 2.23621 | 64.7 | 2.54723 | 72.6 | 2.85826 | 80.5 | 3.16928 | 88.4 | 3.48030 | 96.3 | 3.79133 |
| 56.9 | 2.24015 | 64.8 | 2.55117 | 72.7 | 2.86219 | 80.6 | 3.17322 | 88.5 | 3.48424 | 96.4 | 3.79526 |
| 57.0 | 2.24409 | 64.9 | 2.55511 | 72.8 | 2.86613 | 80.7 | 3.17715 | 88.6 | 3.48818 | 96.5 | 3.79920 |
| 57.1 | 2.24802 | 65.0 | 2.55905 | 72.9 | 2.87007 | 80.8 | 3.18109 | 88.7 | 3.49211 | 96.6 | 3.80314 |
| 57.2 | 2.25196 | 65.1 | 2.56298 | 73.0 | 2.87401 | 80.9 | 3.18503 | 88.8 | 3.49605 | 96.7 | 3.80707 |
| 57.3 | 2.25590 | 65.2 | 2.56692 | 73.1 | 2.87794 | 81.0 | 3.18897 | 88.9 | 3.49999 | 96.8 | 3.81101 |
| 57.4 | 2.25983 | 65.3 | 2.57086 | 73.2 | 2.88188 | 81.1 | 3.19290 | 89.0 | 3.50393 | 96.9 | 3.81495 |
| 57.5 | 2.26377 | 65.4 | 2.57497 | 73.3 | 2.88582 | 81.2 | 3.19684 | 89.1 | 3.50786 | 97.0 | 3.81889 |
| 57.6 | 2.26771 | 65.5 | 2.57873 | 73.4 | 2.88975 | 81.3 | 3.20078 | 89.2 | 3.51180 | 97.1 | 3.82282 |
| 57.7 | 2.27164 | 65.6 | 2.58267 | 73.5 | 2.89369 | 81.4 | 3.20471 | 89.3 | 3.51574 | 97.2 | 3.82676 |
| 57.8 | 2.27558 | 65.7 | 2.58660 | 73.6 | 2.89763 | 81.5 | 3.20865 | 89.4 | 3.51967 | 97.3 | 3.83070 |
| 57.9 | 2.27952 | 65.8 | 2.59054 | 73.7 | 2.90156 | 81.6 | 3.21259 | 89.5 | 3.52361 | 97.4 | 3.83463 |
| 58.0 | 2.28346 | 65.9 | 2.59448 | 73.8 | 2.90550 | 81.7 | 3.21652 | 89.6 | 3.52755 | 97.5 | 3.83857 |
| 58.1 | 2.28739 | 66.0 | 2.59842 | 73.9 | 2.90944 | 81.8 | 3.22046 | 89.7 | 3.53148 | 97.6 | 3.84251 |
| 58.2 | 2.29133 | 66.1 | 2.60235 | 74.0 | 2.91338 | 81.9 | 3.22440 | 89.8 | 3.53542 | 97.7 | 3.84644 |
| 58.3 | 2.29527 | 66.2 | 2.60629 | 74.1 | 2.91731 | 82.0 | 3.22834 | 89.9 | 3.53936 | 97.8 | 3.85038 |
| 58.4 | 2.29920 | 66.3 | 2.61023 | 74.2 | 2.92125 | 82.1 | 3.23227 | 90.0 | 3.54330 | 97.9 | 3.85432 |
| 58.5 | 2.30314 | 66.4 | 2.61416 | 74.3 | 2.92519 | 82.2 | 3.23621 | 90.1 | 3.54723 | 98.0 | 3.85826 |
| 58.6 | 2.30708 | 66.5 | 2.61810 | 74.4 | 2.92912 | 82.3 | 3.24015 | 90.2 | 3.55113 | 98.1 | 3.86219 |
| 58.7 | 2.31101 | 66.6 | 2.62204 | 74.5 | 2.93300 | 82.4 | 3.24408 | 90.3 | 3.55611 | 98.2 | 3.86613 |
| 58.8 | 2.31495 | 66.7 | 2.62597 | 74.6 | 2.93700 | 82.5 | 3.24802 | 90.4 | 3.55904 | 98.3 | 3.87007 |
| 58.9 | 2.31889 | 66.8 | 2.62991 | 74.7 | 2.94093 | 82.6 | 3.25196 | 90.5 | 3.56298 | 98.4 | 3.87400 |
| 59.0 | 2.32283 | 66.9 | 2.63385 | 74.8 | 2.94487 | 82.7 | 3.25589 | 90.6 | 3.56692 | 98.5 | 3.87794 |
| 59.1 | 2.32676 | 67.0 | 2.63779 | 74.9 | 2.94881 | 82.8 | 3.25983 | 90.7 | 3.57085 | 98.6 | 3.88188 |
| 59.2 | 2.33070 | 67.1 | 2.64172 | 75.0 | 2.95275 | 82.9 | 3.26377 | 90.8 | 3.57479 | 98.7 | 3.88581 |
| 59.3 | 2.33464 | 67.2 | 2.64566 | 75.1 | 2.95668 | 83.0 | 3.26771 | 90.9 | 3.57873 | 98.8 | 3.88975 |
| 59.4 | 2.33857 | 67.3 | 2.64960 | 75.2 | 2.96062 | 83.1 | 3.27164 | 91.0 | 3.58267 | 98.9 | 3.89369 |
| 59.5 | 2.34251 | 67.4 | 2.65353 | 75.3 | 2.96456 | 83.2 | 3.27558 | 91.1 | 3.58660 | 99.0 | 3.89763 |
| 59.6 | 2.34645 | 67.5 | 2.65747 | 75.4 | 2.96849 | 83.3 | 3.27952 | 91.2 | 3.59054 | 99.1 | 3.90156 |
| 59.7 | 2.35038 | 67.6 | 2.66141 | 75.5 | 2.97243 | 83.4 | 3.28845 | 91.3 | 3.59448 | 99.2 | 3.90550 |
| 59.8 | 2.35432 | 67.7 | 2.66534 | 75.6 | 2.97637 | 83.5 | 3.28739 | 91.4 | 3.59841 | 99.3 | 3.90944 |
| 59.9 | 2.35826 | 67.8 | 2.66928 | 75.7 | 2.98030 | 83.6 | 3.29133 | 91.5 | 3.60235 | 99.4 | 3.91337 |
| 60.0 | 2.36220 | 67.9 | 2.67322 | 75.8 | 2.98424 | 83.7 | 3.29526 | 91.6 | 3.60629 | 99.5 | 3.91731 |
| 60.1 60.2 60.3 60.4 | 2.36613 2.37007 2.37401 2.37794 | 68.0 68.1 68.2 68.3 | 2.67716 2.68109 2.68503 2.68897 | 75.9 76.0 76.1 76.2 | 2.98818 2.99212 2.99605 2.99999 | 83.8 83.9 84.0 84.1 | 3.29920 3.30314 3.30708 3.31101 | 91.7 91.8 91.9 92.0 | 3.61022 3.61416 3.61810 3.62204 | 99.6 99.7 99.8 99.9 100.0 | 3.92125 3.92518 3.92912 3.93306 3.93700 |

STEEL IDENTIFICATION OF COMPOSITION

The SAE (Society of Automotive Engineers) system of using numbers to designate steel composition is the most widely used and best understood. The AISI (American Iron and Steel Institute) system is also becoming widely used but it does not cause any confusion as both systems use the same numbers.

The systems use four numerals (five numerals are

necessary when the carbon content is 1.00% or higher) each of which designate the basic type. The first digit designates the basic analysis group, the second digit signifies the amount of alloys, and the last two indicate the carbon content. (The last three when carbon is over 1.00%.) In the table below X is substituted for the proper digits.

| Series Designation (1952) | Types and Classes |
|------------------------------|--|
| 10 XX | Carbon Steels — Not Resulphurized |
| *11XX | Carbon Steels — Resulphurized |
| 12 XX | Carbon Steels — Rephosphorized and Resulphurized |
| 13XX | 1.75% Manganese Steels |
| 23XX | 3.50% Nickel Steels |
| 25XX | 5.00% Nickel Steels |
| 31 XX | 1.25% Nickel — .65 or .80% Chromium Steels |
| 33XX | 3.50% Nickel — 1.55% Chromium Steels |
| 40XX | .25% Molybdenum Steels |
| 41XX | .95% Chromium — .20% Molybdenum Steels |
| 43XX | 1.80% Nickel — .50 or .80% Chromium — .25% Molybdenum Steels |
| 46XX | 1.80% Nickel — .25% Molybdenum Steels |
| 48XX | 3.50% Nickel — .25% Molybdenum Steels |
| 50XX | .30 or .60% Chromium Steels |
| 51 XX | .80 or .95% Chromium Steels |
| 51XXX | 1.00% Carbon — 1.00% Chromium Steels |
| 52XXX | 1:00% Carbon — 1.45% Chromium Steels |
| 61 XX | .80 or .95% Chromium — .10 or .15% Vanadium Steels |
| 86XX | .55% Nickel — .50% Chromium — .20% Molybdenum Steels |
| 87XX | .55% Nickel — .50% Chromium — .25% Molybdenum Steels |
| 92XX | .85% Manganese — 2.00% Silicon Steels |
| 94XX | 1.00% Manganese — .45% Nickel — .40% Chromium — .20% Molybdenum Steels |
| 97XX | .55% Nickel — .17% Chromium — .20% Molybdenum Steels |
| 98XX | 1.00% Nickel — .80% Chromium — .25% Molybdenum Steels |

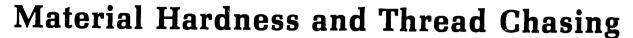
phorized and resulphurized. They are rapidly being replaced by the 1212 and 1213 which are the same composition made by the basic open hearth process. All other 11XX series are resulphurized basic open hearth steels.

The AISI system uses prefix letters to denote method of manufacture. If used the letters are applied as follows:

- C Denotes Basic Open Hearth Carbon Steel (C1020)
- E Denotes Electric Furnace Carbon and Alloy Steel (E4640)
- B Denotes Acid Bessemer Steel (B1112)

The AISI also uses a system for designating standard stainless and heat resisting steels. This system consists of three digits with the first digit either 3 or 4. The 3XX group are all basically Chromium nickel alloys and the 4XX group are straight chromium alloys. The 3XX

group (Example 302, 303, etc.) are austenitic alloys, non-hardenable and are subject to cold work in any machining operation. The 4XX group vary in properties as some are hardenable (Example 416,440A) and others are not. (Example 430,446).

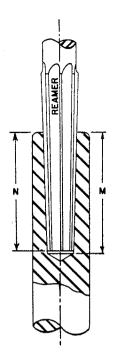


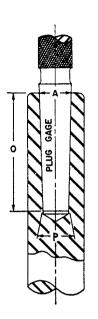
It should be mentioned that the probable tool life column below indicates life relative to hardness only. When considering thread chaser life, all the possible variables relative to the specific application should be considered. Included in these would be the material, thread configuration, lubricant, speed, and general machine conditions under which the thread is to be generated.

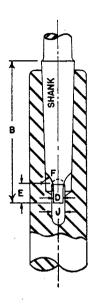
| Brinell | (C Scale) Rockwell | Approximate Tensile Strength In 1000 PSI | Probable Tool Life |
|---------|-----------------------|--|----------------------------|
| 388 | 42 | 195 | Thread Chasing Impractical |
| 375 | 40 | 182 | |
| 363 | 39 | 177 | |
| 353 | 38 | 171 | |
| 341 | 37 | 164 | |
| 331 | 36 | 162 | Premium High Speed |
| 321 | 35 | 155 | Chasers Can Be |
| 311 | 34 | 153 | Supplied, But Tool Life |
| 302 | 32.5 | 144 | Will Be Limited. |
| 293 | 31 | 140 | |
| 285 | 30 | 136 | Tool Life In This |
| 277 | 29 | 132 | Hardness Area Will |
| 269 | 28 | 128 | Generally Be Fair To Good. |
| 262 | 26 | 124 | • |
| 255 | 25 | 121 | |
| 248 | 24 | 117 | |
| 241 | 23 | 115 | Tool Life In This |
| 235 | 21.7 | 111 | Hardness Area Will |
| 230 | 18 | 109 | Generally Range From |
| 223 | 16 | 108 | Good To Excellent. |
| 217 | 14 | 103 | · |
| 212 | | 101 | 1. |
| 207 | | 98 | |
| 201 | | 96 | |

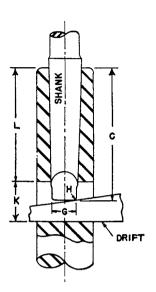
GEOMETRIC TOOL offers various surface treatments at a minimal cost to improve the overall performance of threading chasers for different materials and applications.

STANDARD MORSE TAPERS









| L L | be . | | SHANK | | | | TANG | | | | | TANG SLOT | | | | | | |
|-----------------|-------------------------------|------------------------|-----------------|--------|--------------------------|-------------------------|------------------------|-----------|--------|--------|----------|--------------|-------|--------|-------------------------------|-------------------|-------------------|-----------------|
| Number of Taper | Diam. of Plug at Small End | Diam. at Gauge Line | Whole Length | Depth | Depth of Drilled Hole | Depth of Reamed Hole | Standard Plug Depth | Thickness | Length | Radius | Diameter | Radius | Width | Length | End of Socket to Tang Slot | Taper per Inch | Taper per Foot | Number of Drift |
| | P | A | В | С | М | N | 0 | D | E | F | G | Н | J | K | L | | | |
| *0 | .252 | .356 | 211/32 | 2 7/32 | 2 1/16 | 2 1/32 | 2 | .156 | 1/4 | 5/32 | 15/64 | 3/64 | .166 | 9/16 | 115/16 | .052000 | .62400 | *0 |
| 1 | .369 | .475 | 2 %16 | 2 7/16 | 2 3/16 | 2 5/32 | 2 1/8 | .203 | 3∕8 | 3/16 | 11/32 | 3/64 | .213 | 3/4 | 21/16 | .049882 | .59858 | 1 |
| 2 | .572 | .700 | 3 1/8 | 215/16 | 22 1/32 | 239/64 | 29/16 | .250 | 7/16 | 1/4 | 17/32 | 1/16 | .260 | 7∕8 | 2 ½ | .049951 | .59941 | 2 |
| 3 | .778 | .938 | 3 7/8 | 311/16 | 3 5/16 | 3 1/4 | 33/16 | .312 | 9/16 | 9⁄32 | 23/32 | 5/64 | .322 | 13/16 | 3 1/16 | .050196 | .60235 | 3 |
| 4 | 1.020 | 1.231 | 4 7/8 | 4 % | 4 3/16 | 4 1/8 | 41/16 | .469 | 5⁄8 | 5/16 | 31/32 | 3/32 | `.479 | 1 1/4 | 3 7/8 | .051938 | .62326 | 4 |
| 5 | 1.475 | 1.748 | 6 1/8 | 5 1/8 | 5 5/16 | 5 1/4 | 53/16 | .625 | 3⁄4 | 3/8 | 113/32 | 1/8 | .635 | 1 ½ | 415/16 | .052626 | .63151 | 5 |
| 6 | 2.116 | 2.494 | 8 %16 | 8 1/4 | 713/32 | 72 1/ ₆₄ | 7 1/4 | .750 | 1 1/8 | 1/2 | 2 | 5/32 | .760 | 1 3/4 | 7 | .052137 | .62565 | 6 |
| 7 | 2.750 | 3.270 | 11 % | 11 1/4 | 10 5/32 | 10 5/64 | 10 | 1.125 | 1 % | 3/4 | 2 5/8 | 3/16 | 1.135 | 2 % | 9 ½ | .05200 | .6240 | 7 |

The dimensions agree essentially with dimensions of the American Standard on Machine tapers.

The undercut shown on the tang having diameter G, and length E, may be eliminated at the option of the manufacturer provided the tang is heat-treated to a minimum Rockwell of C30 with 150Kg load.

TO DETERMINE MINOR DIAMETER OF THREAD

D=Major Diameter
D1=Minor Diameter
C=Double Depth of Thread
D1=D-C

TABLE SHOWING DOUBLE DEPTH OF THREADS

| | Amer. Nat'l | Theoretical | | | М | etric |
|--|---|--|---|---|--|---|
| T.P.I. | (U.S.) | V Thread | Whit. | Acme | MM Pitch | Double Depth |
| 3 31/2 4 41/2 5 6 7 71/2 8 9 10 11 111/2 13 14 15 16 17 18 19 20 21 22 24 26 27 28 30 32 24 26 27 28 30 32 34 36 38 40 42 44 46 48 50 52 56 60 64 68 72 74 76 80 | .4330 .3712 .3248 .2887 .2598 .2165 .1856 .1732 .1624 .1443 .1299 .1181 .1130 .1083 .0999 .0928 .0866 .0812 .0764 .0722 .0684 .0650 .0619 .0590 .0541 .0500 .0446 .0433 .0406 .0382 .0325 .0309 .0295 .0295 .0295 .0295 .0295 .0295 .0295 .0295 .0295 .0295 .0297 .0296 .0217 .0200 .0217 .0203 .0191 .0180 .0175 .0171 .0162 | .5773 .4948 .4330 .3849 .3464 .2887 .2474 .2309 .2165 .1924 .1732 .1575 .1506 .1443 .1332 .1237 .1155 .1083 .1019 .0962 .0912 .0866 .0825 .0787 .0722 .0666 .0642 .0618 .0577 .0541 .0509 .0481 .0456 .0433 .0412 .0394 .0377 .0361 .0394 .0377 .0361 .0394 .0377 .0361 .0394 .0377 .0361 .0399 .0289 .0271 .0228 .0217 | .4269 .3659 .3202 .2846 .2561 .2134 .1830 .1708 .1601 .1423 .1281 .1164 .1114 .1067 .0985 .0915 .0854 .0800 .0753 .0711 .0674 .0640 .0610 .0582 .0534 .0493 .0474 .0457 .0427 .0400 .0377 .0356 .0337 .0320 .0305 .0291 .0278 .0267 .0256 .0246 .0229 .0213 .0200 .0188 .0178 .0173 .0169 .0160 | .3533 .3057 .2700 .2422 .2200 .1867 .1629 .1533 .1450 .1311 .1200 .1009 .0970 .0933 .0869 .0814 .0767 .0725 .0688 .0656 .0626 | .25 .30 .35 .40 .45 .50 .55 .60 .65 .70 .75 .80 .85 .90 .95 1.0 1.1 1.2 1.25 1.3 1.4 1.5 1.6 1.7 1.75 1.8 1.9 2.0 2.25 2.75 3.0 3.25 3.75 4.0 4.5 5.0 6.5 7.0 7.5 8.0 9.5 10.0 | .0138 .0165 .0193 .0221 .0248 .0276 .0303 .0331 .0358 .0386 .0413 .0441 .0468 .0496 .0524 .0551 .0606 .0661 .0689 .0717 .0772 .0827 .0827 .0982 .0937 .0965 .0992 .1047 .1102 .1240 .1378 .1516 .1654 .1791 .1929 .2067 .2205 .2480 .2756 .3031 .3307 .3583 .3858 .4134 .4409 .4685 .4961 .5236 .5512 |

For use in determining minor diameter of Pipe Threads for the purposes of this Book, use \dot{V} Thread figures.

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